

NATIONAL HIGHWAYS AND INFRASTRUCTURE DEVELOPMENT CORPORATION LIMITED

A GOVT. OF INDIA UNDERTAKING

Consultancy Services for Feasibility Study and Detailed Project Report for Four / Six Laning from Km 38.000 to Km 168.167 of Daboka-Dimapur Section of NH-36 & 39 in the State of Assam & Nagaland under NHDP, Phase – III B, Pkg. No. NHDP – III/DL5/21, Group - G

DIMAPUR BYPASS (ASSAM PART)



REVISED FINAL DETAILED PROJECT REPORT VOLUME III : MATERIAL REPORT



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**DECEMBER
2016**

NATIONAL HIGHWAYS INFRASTRUCTURE DEVELOPMENT CORPORATION LTD.

PREPARATION OF DETAILED PROJECT REPORT FOR
DEVELOPMENT OF NH 36 & NH 39

FROM DOBOKA TO DIMAPUR UNDER PHASE 'B' OF SARDP-NE
(Pkg-I) - Dimapur Bypass (Assam & Nagaland)



FINAL DETAILED PROJECT REPORT
ON
ROAD & PAVEMENT AND MATERIAL INVESTIGATIONS

December, 2016

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1. Introduction

The report presents the results of Pavement investigations and soil & material survey works for the proposed 4- laning from Doboka to Dimapur of NH-36 & 39 in the state of Assam and Nagaland. The road starts from Km 38.000 and end at Km 168.167 of NH 36. It meets NH-39 at Km 124.200 the Bypass Starts at Km 118.050 of NH-36 & ends at 153.058 (Both Design Chainages)

The investigation was conducted via site visit, collection of representative material, testing the samples both in the field and laboratory.

All samples from the respective test locations were brought to the laboratory at Guwahati established where they were further examined and were subjected to specified and required testing.

1.1: Purpose and Scope

The purpose and scope of our services were as follows:

a) To determine the characteristics and strength of the subgrade along the existing road.

The tests included to accomplish these are as follows:

- In-situ density and moisture content at each test pit.
- Field CBR using DCP at each test pit..
- Modified Proctor tests to determine maximum dry density and optimum moisture content of the subgrade soil in the laboratory.
- Characterization (grain size and Atterberg Limits) of subgrade soil.
- Laboratory CBR (both unsoaked and 4-day soaked) at three energy level.

b) Determination of Pavement Composition i.e. material type and corresponding thickness of different layers / composition of Pavement. The side of test pits should be cleaned properly and thickness of each individual layers of pavement to be measured and recorded in the field.

c) To evaluate the suitability of borrow material for use in construction of embankment and/or subgrade and location of borrow area.

The laboratory tests included under this are as follows:

- Sieve Analysis
- Liquid and Plastic Limits
- Soil Classification
- MDD and OMC
- CBR at three energy level

d) To locate the quarries and testing of stone aggregate as available to evaluate their suitability for use in construction of Pavement, such as Wet Mix Macadam (WMM), Dense Bituminous Macadam (DBM), Bituminous Concrete and Cement Concrete.

The tests included under this are as follows:

- Sieve analysis
- Flakiness and Elongation Index
- Specific Gravity and Water Absorption
- Aggregate Impact Value
- Stripping Value
- Soundness

e) Testing of available sand in the close proximity of the existing highway for use in bituminous mixtures and cement concrete work.

The tests included to determine the suitability of fine aggregates are as follows:

- Sieve analysis
- Fineness Modules
- Specific gravity
- Deleterious content

In order to accomplish this purpose, we have performed the required and all necessary field work and laboratory tastings as follows:

f) Testing of available water to determine their suitability for various types of works and determine their adequacy for construction activities.

In order to accomplish this purpose, we have performed the required and all necessary field work and laboratory tastings as follows:

- PH Value
- Suspended matter
- Chemical Constituents of Chloride, Sulphate
- Organise / Inorganise matters.

■ **Field density Test:**

Field density test was conducted by the core cutter method as guided by IS 2720-1996 (Part XXVII) at the subgrade of each test pit.

Laboratory Investigations:

The following laboratory tests were carried out on representative samples by following relevant IS Code:

- **Atterberg Limits (IS:2720-Part 5) :**
The liquid and plastic limits of soils, which are cohesive in nature, were determined to classify the soil and qualitatively assess their consistency and compressibility.
- **Natural Moisture Content (IS:2720-Part 2) :**
Natural moisture content of the representative samples were found to determine the dry density and to study the degree of compressibility of the subgrade soil.
- **Grain Size Distribution (IS:2720 Part 4) :**
Sieve analysis were performed on soil samples collected from test pits and borrow area to study the compaction characteristics and their suitability as to their use as construction material for embankment and / or subgrade.
- **Modified Proctor Test (IS:2720 Part 8) :**
Modified proctor test gives the higher degree of compaction. In this test, the soil is compacted in Standard Proctor Mould (capacity 1/30 cu. Ft. or 945ml) but in 5 layers being given 25 blows of 4.5kg rammer dropped from a height of 450mm. This test determines the maximum dry density of the soil and corresponding optimum moisture content. These parameters are used to find the degree of compaction of subgrade soil of the existing pavement and also to determine the compaction criteria to be followed to assure the quality of compaction during construction of embankment and / or preparation of subgrade. The results of all modified proctor tests are presented here is in this report.
- **California bearing ratio test (IS:2720-Part 16) :**
California bearing ratio tests were performed on bulk samples collected from pavement subgrade of existing highway, from new alignment of widening portion and on borrow materials. The CBR was determined for 3 energy level on both unsoaked and 4 days soaked conditions. To achieve the required CBR of 7, the compaction criteria to be required were also studied. The results of all CBR Tests are shown in tabular form in the later part of this report.

a) Material Investigation :

The material commonly used in highway embankment, subgrade and pavement comprise of soil, gravel (both water borne and pit), stone metal. So it is very important as well as necessary to identify the potential source in substantial quantity of these materials near or in the close vicinity of the construction area.

All representative samples as collected from different borrow area and quarries were brought to the laboratory at Guwahati and were subjected to appropriate and specified laboratory tastings to evaluate their suitability for various components of work and to establish quality and quantity of these material and recommendations as to their use.

Mass haul diagram for haulage purpose are prepared indicating location of selected borrow area, quarries and estimated available quantity.

i) Borrow Area Soil:

Survey was conducted to locate the potential source of borrow area soil required for the construction of embankment and subgrade. The distance from the highway to these borrow areas are shown in the lead chart and is attached in this report. The laboratory tests as detailed earlier in this report were conducted on all samples and the results of which are shown in the attached plates.

i) Laboratory Tests of Aggregates:

a) Coarse Aggregates:

- Sieve Analysis : (IS:383-1997)
- Flakiness and Elongation Index : (IS:2386 Part 1)
- Specific gravity and water absorption : (IS:2386 Part 3)
- Aggregate Impact Value (AIV) : (IS:2386 Part 5)
- Stripping Values
- Soundness

Discussion and Evaluations

The investigations were performed by conducting in-situ testing and supplemented by laboratory testing and measurement of existing pavement thickness. In addition to this, sub grade soil along the widening portion, borrow materials, such as soil and aggregates were tested in the laboratory for evaluation as to their suitability for their use in construction of the proposed highway.

In general the test data reveal that the in-situ field dry density at the existing pavement subgrade varies in the range of 1.54 to 1.80 gms/cc, the laboratory MDD varies in the range of 1.72 to 1.60 gm/cc and the corresponding laboratory CBR values vary in the range 4 to 6 for lowest energy level, 5 to 8 for mid energy level and 6 to a maximum of 12 for the highest energy level.

2. PAVEMENT INVESTIGATION

2.1 General

The existing project road is a flexible pavement and is in poor condition in some stretches. There are a few low laying sections along the road from heavy rains during monsoons. The water stagnates along road side damaging the subgrade and pavement component layers.

2.2 Existing Pavement Composition

The Project road NH-36 is in a poor condition although the pavement comprises of a severely worn out wearing course (PC), a base course (WBM) and stone soling.

The crust thickness and the type of pavement layers were recorded and are given in Table-2.1. The average thickness of the pavement component layers is presented in Tables of Pavement Condition Survey.

2.3 Pavement Condition Survey

The pavement condition survey was carried out by visual means supplemented by measurements as per the guidelines mentioned in IRC: SP: 19 – 2001. Detailed field study included pavement condition, shoulder condition, embankment condition, drainage condition etc. The existing pavement conditions were identified and the results have been summarized for every km interval sectional length of the project roads in Table-2.1

The condition of existing road was measured for cracks, releveling, potholes, patching, present of rut and pavement edges drop.

The Riding Quality, in terms of (i) Speed (in km/hr) and (ii) quality (Good, Fair, Poor, Very Poor).

Route depth was measured transversely across the outer wheel paths using 3m long straight edge and graduated wedge.

Shoulder and embankment conditions were observed by visual means and the existence of distress, its cause and extent were noted. Nearly 65% was observed as felled and remaining as in fair condition. The results of Pavement Condition Survey in each km are summarized in the Tables-2.1.

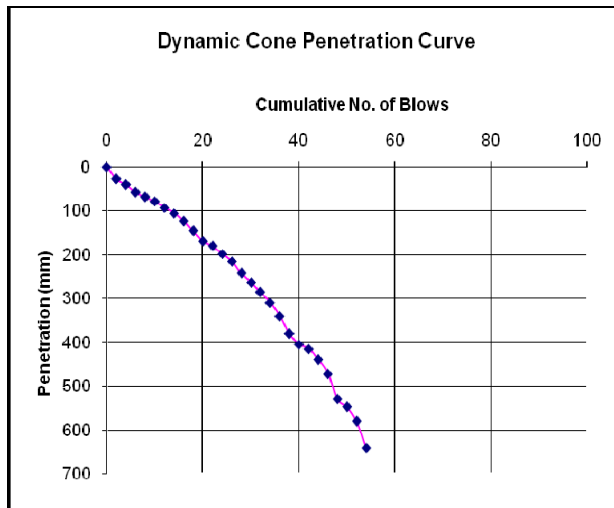
| Table No.:2.1 | | | | | | | | | | |
|---------------|----------------------|----------|----------------|----------------|----------------------|---------|--------|-------|----------------------|---------------------------|
| Pit Reference | Pavement Composition | | | Sub grade type | *Soil Classification | LL | PL | PI | Moisture Content (%) | Field Dry Density (gm/cc) |
| | GSB (MM) | WBM (MM) | BITUMINOUS(MM) | | | | | | | |
| 40+100 | 0 | 180 | 60 | Silty Clay | CL | 34.53 | 27.39 | 7.14 | 19 | 0.19 |
| 45+150 | 0 | 180 | 60 | Silty Clay | CL | 36.834 | 25.522 | 11.31 | 11 | 0.12 |
| 50+100 | 0 | 180 | 60 | Silty Clay | CL | 30.014 | 22.452 | 7.56 | 8 | 0.14 |
| 55+200 | 0 | 180 | 60 | Silty Clay | CL | 28.564 | 21.212 | 7.35 | 9 | 0.10 |
| 60+100 | 0 | 180 | 65 | Silty Clay | CL | 30.114 | 21.002 | 9.11 | 11 | 0.08 |
| 65+000 | 0 | 200 | 65 | Silty Clay | CL | 28.854 | 22.622 | 6.23 | 12 | 0.11 |
| 70+000 | 0 | 200 | 75 | Silty Clay | CL | 26.364 | 19.232 | 7.13 | 13 | 0.15 |
| 75+100 | 0 | 200 | 75 | Silty Clay | CL | 28.344 | 21.422 | 6.92 | 5 | 0.06 |
| 80+200 | 0 | 200 | 60 | Silty Clay | CL | 29.524 | 21.412 | 8.11 | 8 | 0.09 |
| 85+000 | 0 | 200 | 60 | Silty Clay | CL | 28.654 | 22.212 | 6.44 | 9 | 0.10 |
| 90+000 | 0 | 200 | 60 | Silty Clay | CL | 27.37 | 20.33 | 7.04 | 11 | 0.12 |
| 95+400 | 0 | 200 | 60 | Silty Clay | CL | 28.3642 | 20.002 | 8.36 | 17 | 0.20 |
| 100+200 | 0 | 200 | 70 | Silty Clay | CL | 29.7642 | 21.232 | 8.53 | 15 | 0.18 |
| 105+250 | 0 | 200 | 70 | Silty Clay | CL | 29.4142 | 20.052 | 9.36 | 19 | 0.22 |
| 110+100 | 0 | 200 | 70 | Silty Clay | CL | 30.0442 | 22.342 | 7.70 | 18 | 0.20 |
| 115+500 | 0 | 0 | 0 | Silty Clay | CL | 28.4242 | 19.732 | 8.69 | 26 | 0.29 |
| 120+000 | 0 | 0 | 0 | Silty Clay | CL | 26.8742 | 20.242 | 6.63 | 17 | 0.20 |
| 125+150 | 0 | 180 | 75 | Silty Clay | CL | 27.3342 | 19.502 | 7.83 | 12 | 0.14 |
| 130+100 | 0 | 180 | 75 | Silty Clay | CL | 28.4142 | 20.012 | 8.40 | 12 | 0.14 |
| 135+100 | 0 | 180 | 75 | Silty Clay | CL | 27.3542 | 19.552 | 7.80 | 16 | 0.18 |
| 140+350 | 0 | 180 | 60 | Silty Clay | CL | 28.0342 | 19.792 | 8.24 | 9 | 0.10 |
| 145+100 | 0 | 180 | 60 | Silty Clay | CL | 29.7142 | 20.032 | 9.68 | 21 | 0.23 |
| 150+550 | 0 | 180 | 60 | Silty Clay | CL | 30.5542 | 22.282 | 8.27 | 11 | 0.13 |
| 155+000 | 0 | 180 | 45 | Silty Clay | CL | 32.2342 | 23.512 | 8.72 | 21 | 0.20 |
| 160+000 | 0 | 250 | 45 | Silty Clay | CL | 28.54 | 22.2 | 6.34 | 10 | 0.11 |
| 165+000 | 0 | 250 | 65 | Silty Clay | CL | 27.53 | 19.85 | 7.68 | 13 | 0.16 |

3. DYNAMIC CONE PENETRATION TEST

It is simple device for investigating the compactness of the sub soil layer without making bore hole. The data obtain by this test provides a continuous record of soil resistance. The test is quick and the penetration values may be used for determination of bearing capacity.

FIELD TEST RESULTS

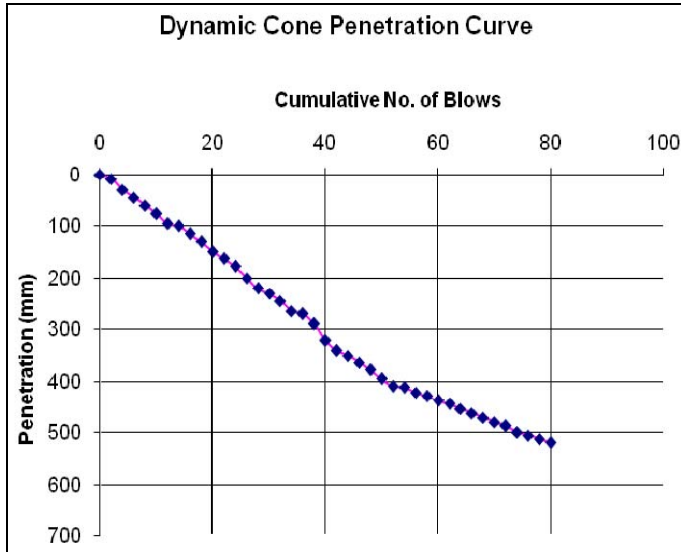
FIELD TEST RESULT AT CHAINAGE=40.100KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 27 |
| 4 | 40 |
| 6 | 57 |
| 8 | 68 |
| 10 | 78 |
| 12 | 92 |
| 14 | 105 |
| 16 | 123 |
| 18 | 145 |
| 20 | 168 |
| 22 | 180 |
| 24 | 198 |
| 26 | 215 |
| 28 | 242 |
| 30 | 263 |
| 32 | 285 |
| 34 | 310 |
| 36 | 340 |
| 38 | 380 |
| 40 | 405 |
| 42 | 416 |
| 44 | 440 |
| 46 | 472 |
| 48 | 530 |
| 50 | 548 |
| 52 | 580 |
| 54 | 642 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 9 | 35 |
| 200-400 | 10 | 29 |
| 400-600 | 10 | 25 |

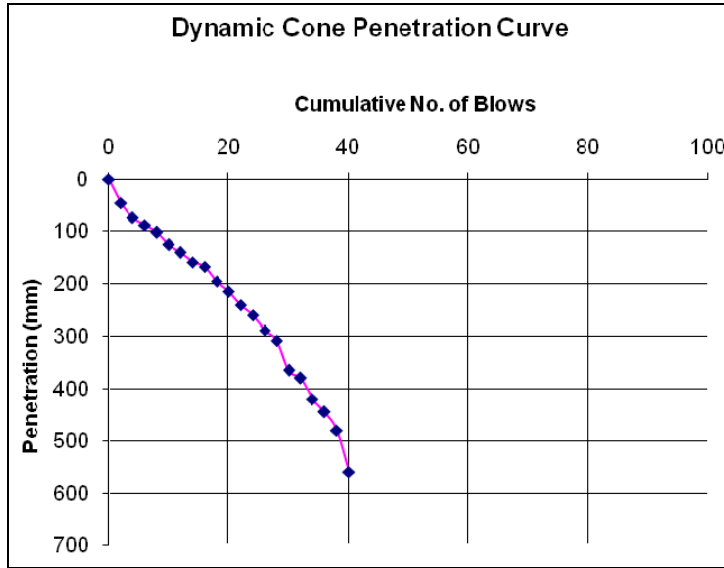
FIELD TEST RESULT AT CHAINAGE=50.150KM



| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 10 | 39 |
| 200-400 | 9 | 40 |
| 400-600 | 8 | 42 |

| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 8 |
| 4 | 30 |
| 6 | 45 |
| 8 | 60 |
| 10 | 76 |
| 12 | 96 |
| 14 | 100 |
| 16 | 115 |
| 18 | 130 |
| 20 | 148 |
| 22 | 163 |
| 24 | 178 |
| 26 | 200 |
| 28 | 221 |
| 30 | 231 |
| 32 | 245 |
| 34 | 265 |
| 36 | 270 |
| 38 | 290 |
| 40 | 322 |
| 42 | 341 |
| 44 | 351 |
| 46 | 364 |
| 48 | 378 |
| 50 | 395 |
| 52 | 410 |
| 54 | 412 |
| 56 | 422 |
| 58 | 430 |
| 60 | 438 |
| 62 | 445 |
| 64 | 454 |
| 66 | 463 |
| 68 | 472 |
| 70 | 480 |
| 72 | 488 |
| 74 | 500 |
| 76 | 506 |
| 78 | 512 |
| 80 | 520 |

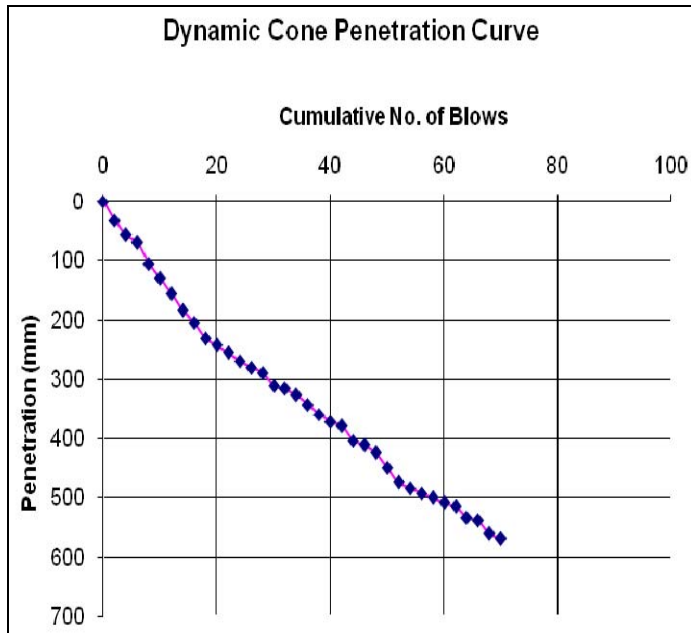
FIELD TEST RESULT AT CHAINAGE=60.000KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 45 |
| 4 | 74 |
| 6 | 88 |
| 8 | 102 |
| 10 | 126 |
| 12 | 141 |
| 14 | 159 |
| 16 | 168 |
| 18 | 196 |
| 20 | 215 |
| 22 | 241 |
| 24 | 261 |
| 26 | 289 |
| 28 | 308 |
| 30 | 365 |
| 32 | 380 |
| 34 | 420 |
| 36 | 445 |
| 38 | 480 |
| 40 | 560 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 10 | 27 |
| 200-400 | 11 | 24 |
| 400-600 | 14 | 19 |

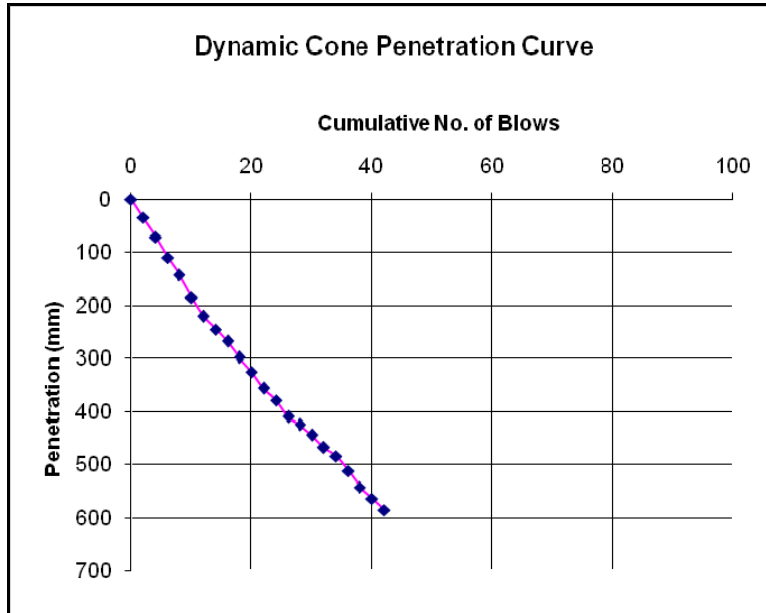
FIELD TEST RESULT AT CHAINAGE=70.120KM



| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 12 | 24 |
| 200-400 | 10 | 33 |
| 400-600 | 9 | 35 |

| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 32 |
| 4 | 57 |
| 6 | 70 |
| 8 | 105 |
| 10 | 130 |
| 12 | 156 |
| 14 | 184 |
| 16 | 205 |
| 18 | 230 |
| 20 | 242 |
| 22 | 255 |
| 24 | 269 |
| 26 | 280 |
| 28 | 289 |
| 30 | 310 |
| 32 | 315 |
| 34 | 326 |
| 36 | 342 |
| 38 | 360 |
| 40 | 372 |
| 42 | 380 |
| 44 | 405 |
| 46 | 412 |
| 48 | 425 |
| 50 | 450 |
| 52 | 475 |
| 54 | 485 |
| 56 | 493 |
| 58 | 501 |
| 60 | 509 |
| 62 | 516 |
| 64 | 534 |
| 66 | 539 |
| 68 | 561 |
| 70 | 570 |

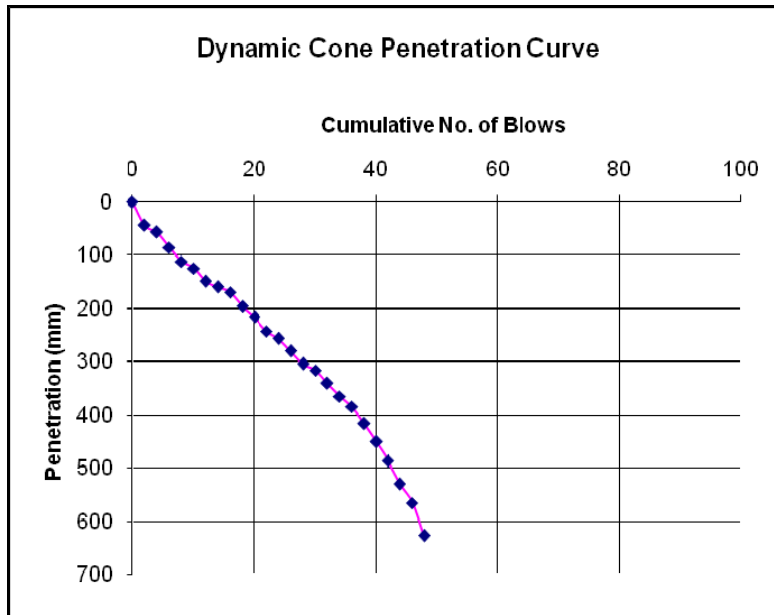
FIELD TEST RESULT AT CHAINAGE=80.000KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 35 |
| 4 | 71 |
| 6 | 110 |
| 8 | 143 |
| 10 | 185 |
| 12 | 221 |
| 14 | 245 |
| 16 | 268 |
| 18 | 298 |
| 20 | 325 |
| 22 | 356 |
| 24 | 379 |
| 26 | 410 |
| 28 | 425 |
| 30 | 445 |
| 32 | 468 |
| 34 | 485 |
| 36 | 512 |
| 38 | 543 |
| 40 | 564 |
| 42 | 586 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 18 | 14 |
| 200-400 | 15 | 17 |
| 400-600 | 13 | 22 |

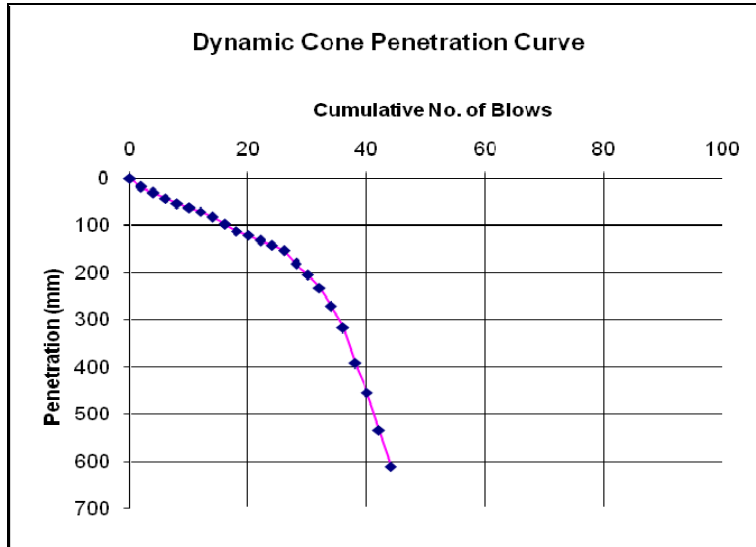
FIELD TEST RESULT AT CHAINAGE=90.000KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 44 |
| 4 | 57 |
| 6 | 86 |
| 8 | 112 |
| 10 | 125 |
| 12 | 150 |
| 14 | 160 |
| 16 | 170 |
| 18 | 196 |
| 20 | 216 |
| 22 | 243 |
| 24 | 257 |
| 26 | 281 |
| 28 | 305 |
| 30 | 316 |
| 32 | 341 |
| 34 | 366 |
| 36 | 386 |
| 38 | 417 |
| 40 | 451 |
| 42 | 488 |
| 44 | 531 |
| 46 | 566 |
| 48 | 628 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 12 | 27 |
| 200-400 | 11 | 26 |
| 400-600 | 14 | 24 |

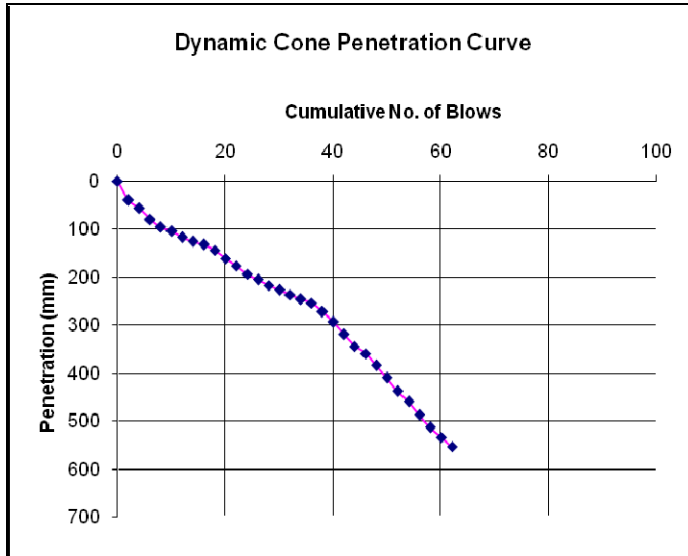
FIELD TEST RESULT AT CHAINAGE=100.100KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 18 |
| 4 | 31 |
| 6 | 43 |
| 8 | 54 |
| 10 | 63 |
| 12 | 71 |
| 14 | 83 |
| 16 | 97 |
| 18 | 112 |
| 20 | 121 |
| 22 | 132 |
| 24 | 142 |
| 26 | 154 |
| 28 | 182 |
| 30 | 204 |
| 32 | 232 |
| 34 | 272 |
| 36 | 317 |
| 38 | 392 |
| 40 | 455 |
| 42 | 534 |
| 44 | 612 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 8 | 38 |
| 200-400 | 11 | 27 |
| 400-600 | 15 | 19 |

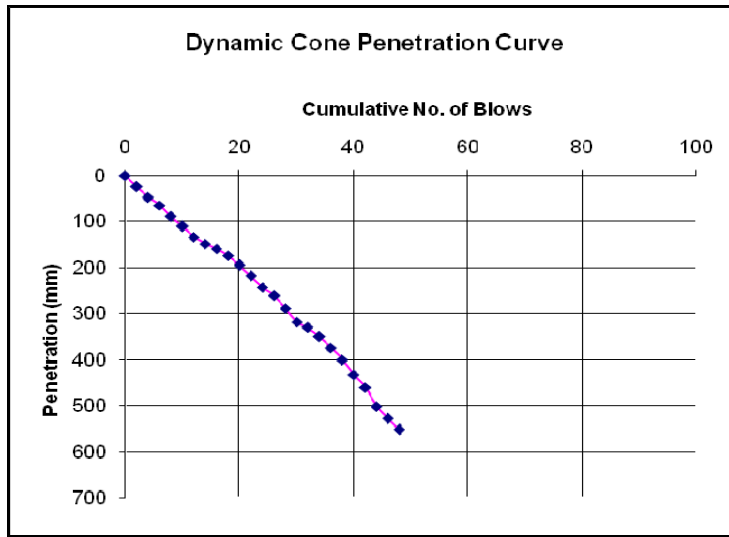
FIELD TEST RESULT AT CHAINAGE=110.000KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 40 |
| 4 | 57 |
| 6 | 80 |
| 8 | 96 |
| 10 | 104 |
| 12 | 117 |
| 14 | 126 |
| 16 | 132 |
| 18 | 144 |
| 20 | 161 |
| 22 | 176 |
| 24 | 194 |
| 26 | 206 |
| 28 | 217 |
| 30 | 227 |
| 32 | 237 |
| 34 | 247 |
| 36 | 254 |
| 38 | 272 |
| 40 | 294 |
| 42 | 320 |
| 44 | 344 |
| 46 | 360 |
| 48 | 384 |
| 50 | 410 |
| 52 | 438 |
| 54 | 460 |
| 56 | 488 |
| 58 | 514 |
| 60 | 534 |
| 62 | 554 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 9 | 35 |
| 200-400 | 10 | 34 |
| 400-600 | 11 | 30 |

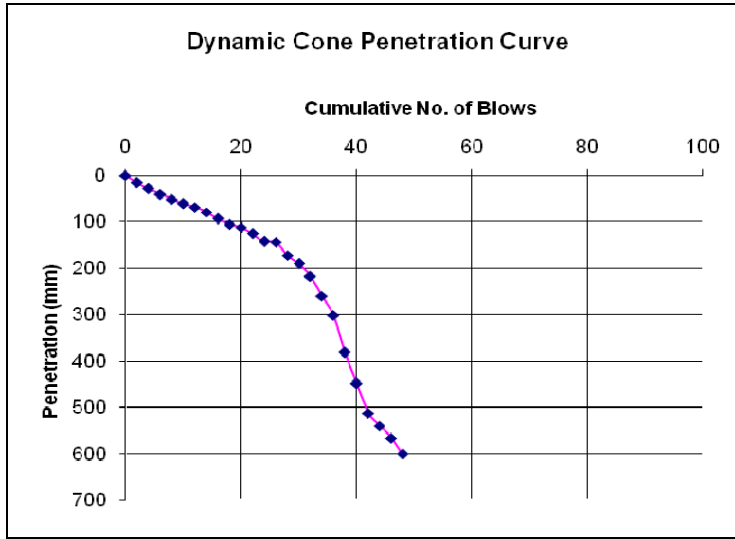
FIELD TEST RESULT AT CHAINAGE=120.200KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 25 |
| 4 | 47 |
| 6 | 64 |
| 8 | 89 |
| 10 | 111 |
| 12 | 133 |
| 14 | 149 |
| 16 | 159 |
| 18 | 174 |
| 20 | 195 |
| 22 | 219 |
| 24 | 243 |
| 26 | 261 |
| 28 | 288 |
| 30 | 319 |
| 32 | 330 |
| 34 | 350 |
| 36 | 375 |
| 38 | 400 |
| 40 | 433 |
| 42 | 461 |
| 44 | 502 |
| 46 | 529 |
| 48 | 552 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 10 | 28 |
| 200-400 | 10 | 28 |
| 400-600 | 12 | 25 |

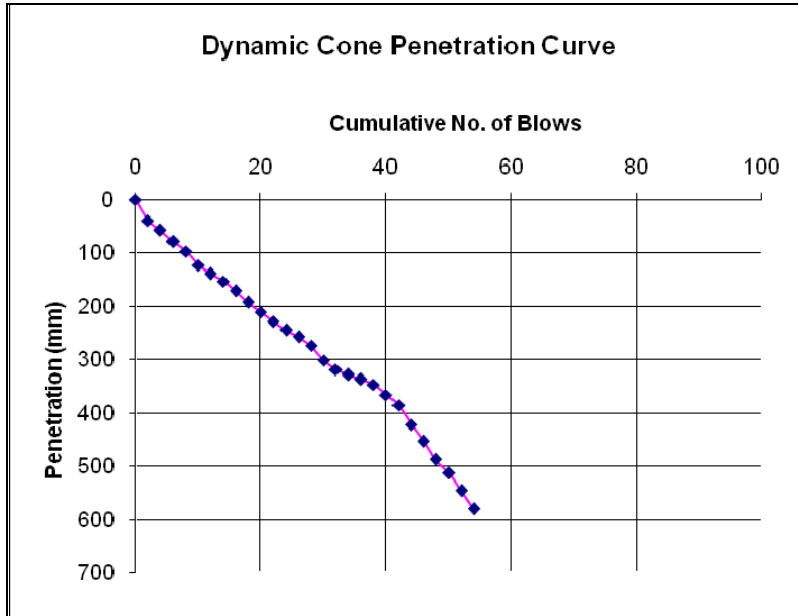
FIELD TEST RESULT AT CHAINAGE=130.000KM



| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 9 | 38 |
| 200-400 | 10 | 27 |
| 400-600 | 12 | 25 |

| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 16 |
| 4 | 29 |
| 6 | 41 |
| 8 | 52 |
| 10 | 61 |
| 12 | 69 |
| 14 | 80 |
| 16 | 94 |
| 18 | 105 |
| 20 | 112 |
| 22 | 126 |
| 24 | 143 |
| 26 | 144 |
| 28 | 172 |
| 30 | 191 |
| 32 | 217 |
| 34 | 260 |
| 36 | 302 |
| 38 | 382 |
| 40 | 449 |
| 42 | 512 |
| 44 | 540 |
| 46 | 566 |
| 48 | 602 |

FIELD TEST RESULT AT CHAINAGE=140.100KM

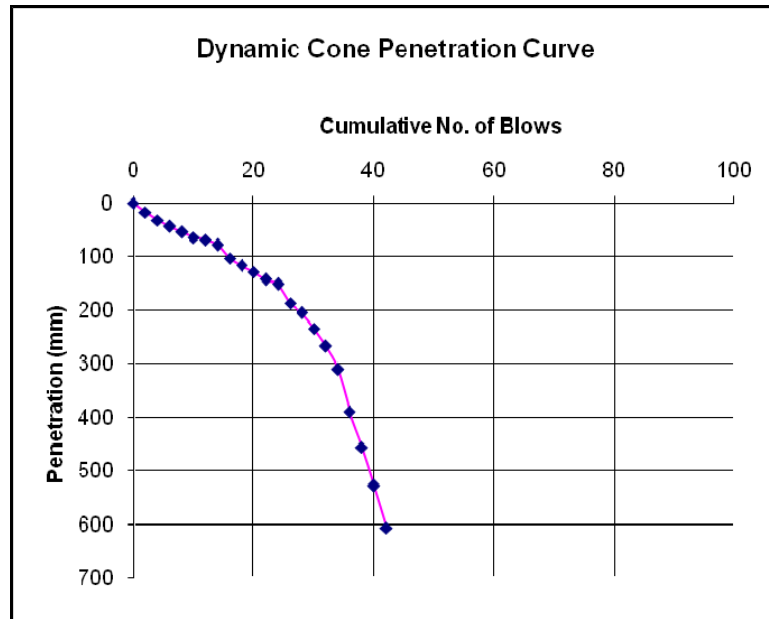


| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 39 |
| 4 | 57 |
| 6 | 79 |
| 8 | 97 |
| 10 | 123 |
| 12 | 139 |
| 14 | 153 |
| 16 | 171 |
| 18 | 193 |
| 20 | 211 |
| 22 | 228 |
| 24 | 244 |
| 26 | 257 |
| 28 | 274 |
| 30 | 301 |
| 32 | 319 |
| 34 | 328 |
| 36 | 337 |
| 38 | 347 |
| 40 | 366 |
| 42 | 386 |
| 44 | 422 |
| 46 | 453 |
| 48 | 488 |
| 50 | 512 |
| 52 | 546 |
| 54 | 580 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 9 | 32 |
| 200-400 | 10 | 30 |
| 400-600 | 12 | 27 |

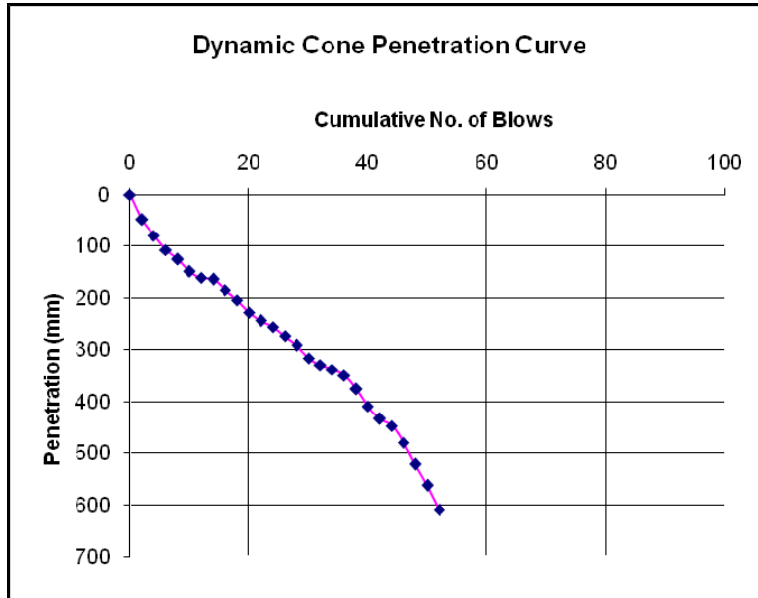
FIELD TEST RESULT AT CHAINAGE=150.000KM

| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 17 |
| 4 | 32 |
| 6 | 44 |
| 8 | 55 |
| 10 | 64 |
| 12 | 69 |
| 14 | 79 |
| 16 | 103 |
| 18 | 117 |
| 20 | 129 |
| 22 | 143 |
| 24 | 152 |
| 26 | 187 |
| 28 | 206 |
| 30 | 235 |
| 32 | 268 |
| 34 | 311 |
| 36 | 391 |
| 38 | 456 |
| 40 | 529 |
| 42 | 607 |



| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 9 | 36 |
| 200-400 | 12 | 25 |
| 400-600 | 14 | 18 |

FIELD TEST RESULT AT CHAINAGE=160.000KM



| cum. No. of blows | Penetration (mm) |
|-------------------|------------------|
| 0 | 0 |
| 2 | 48 |
| 4 | 80 |
| 6 | 108 |
| 8 | 126 |
| 10 | 150 |
| 12 | 162 |
| 14 | 165 |
| 16 | 185 |
| 18 | 205 |
| 20 | 228 |
| 22 | 244 |
| 24 | 256 |
| 26 | 274 |
| 28 | 292 |
| 30 | 316 |
| 32 | 330 |
| 34 | 338 |
| 36 | 349 |
| 38 | 376 |
| 40 | 410 |
| 42 | 434 |
| 44 | 448 |
| 46 | 481 |
| 48 | 522 |
| 50 | 563 |
| 52 | 610 |

| Depth Range | DCP (mm/blow) | CBR (%) |
|-------------|---------------|---------|
| 0-200 | 11 | 26 |
| 200-400 | 12 | 25 |
| 400-600 | 11 | 24 |

4. SAND REPLACEMENT METHOD

Field density test was conducted by the sand replace method as guided by (IS: 2386 Part III)-1988. The equipments are used in the sand replacement method are

- a) Sand pouring cylinder mounted above a pouring cone and separated by a shutter.
- b) Calibrating container
- c) Chisel, scoop, balance etc.

The various test result of different field location are given below

Location: 40.100 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 2.989 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.313 | gm |
| 4 | Weight of sand bottle with sand | 6.691 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.373 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.318 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 908.966 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.001 | gm/cc |
| 13 | Water Content of excavated soil | 19 | % |
| 14 | Dry Density of soil | 0.189 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/16 | |
| wt of empty container= | 12.5 | gm |
| wt of cont. + wet soil= | 75.63 | gm |
| wt of cont. + dry soil = | 65.64 | gm |
| water content of excavated soil= | 19 | % |

Location: 50.150 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.329 | gm |
| 2 | Weight of empty Pan | 1.669 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.66 | gm |
| 4 | Weight of sand bottle with sand | 6.689 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.329 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.359 | gm |
| 7 | Weight of graduated jar | 1.764 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.359 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 937.241 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 20 | % |
| 14 | Dry Density of soil | 0.198 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/27 | |
| wt of empty container= | 13.26 | gm |
| wt of cont. + wet soil= | 56.32 | gm |
| wt of cont. + dry soil = | 49.26 | gm |
| water content of excavated soil= | 20 | % |

Location: 60.000 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.185 | gm |
| 2 | Weight of empty Pan | 1.674 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.508 | gm |
| 4 | Weight of sand bottle with sand | 6.689 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.054 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.635 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 1127.586 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.001 | gm/cc |
| 13 | Water Content of excavated soil | 19 | % |
| 14 | Dry Density of soil | 0.187 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/14 | |
| wt of empty container= | 13.2 | gm |
| wt of cont. + wet soil= | 56.32 | gm |
| wt of cont. + dry soil = | 49.56 | gm |
| water content of excavated soil= | 19 | % |

Location: 70.120 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.316 | gm |
| 2 | Weight of empty Pan | 1.674 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.64 | gm |
| 4 | Weight of sand bottle with sand | 6.689 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.320 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.371 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.358 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.593 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 946.704 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 15 | % |
| 14 | Dry Density of soil | 0.148 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|---------|----|
| container no.= | 110 | |
| wt of empty container= | 21.95 | gm |
| wt of cont. + wet soil= | 120.65 | gm |
| wt of cont. + dry soil = | 108.065 | gm |
| water content of excavated soil= | 15 | % |

Location: 80.000 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.126 | gm |
| 2 | Weight of empty Pan | 1.673 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.451 | gm |
| 4 | Weight of sand bottle with sand | 6.691 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.510 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.181 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 814.483 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 14 | % |
| 14 | Dry Density of soil | 0.142 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/7 | |
| wt of empty container= | 13.65 | gm |
| wt of cont. + wet soil= | 57.85 | gm |
| wt of cont. + dry soil = | 52.41 | gm |
| water content of excavated soil= | 14 | % |

Location: 90.000 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.214 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.526 | gm |
| 4 | Weight of sand bottle with sand | 6.689 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.286 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.405 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 968.966 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 11 | % |
| 14 | Dry Density of soil | 0.116 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/15 | |
| wt of empty container= | 12.85 | gm |
| wt of cont. + wet soil= | 68.45 | gm |
| wt of cont. + dry soil = | 62.74 | gm |
| water content of excavated soil= | 11 | % |

Location: 100.100 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.265 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.589 | gm |
| 4 | Weight of sand bottle with sand | 6.691 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.313 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.374 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 947.586 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 15 | % |
| 14 | Dry Density of soil | 0.154 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|--------|----|
| container no.= | 105 | |
| wt of empty container= | 22.05 | gm |
| wt of cont. + wet soil= | 105.64 | gm |
| wt of cont. + dry soil = | 94.61 | gm |
| water content of excavated soil= | 15 | % |

Location: 110.000 km

| SI No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.156 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.480 | gm |
| 4 | Weight of sand bottle with sand | 6.658 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.451 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.207 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 832.414 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 18 | % |
| 14 | Dry Density of soil | 0.186 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/11 | |
| wt of empty container= | 12.75 | gm |
| wt of cont. + wet soil= | 59.63 | gm |
| wt of cont. + dry soil = | 52.34 | gm |
| water content of excavated soil= | 18 | % |

Location: 120.200 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.465 | gm |
| 2 | Weight of empty Pan | 1.674 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.791 | gm |
| 4 | Weight of sand bottle with sand | 6.689 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.453 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.236 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 852.414 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 10 | % |
| 14 | Dry Density of soil | 0.107 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|--------|----|
| container no.= | 1/2 | |
| wt of empty container= | 12.05 | gm |
| wt of cont. + wet soil= | 58.46 | gm |
| wt of cont. + dry soil = | 54.068 | gm |
| water content of excavated soil= | 10 | % |

Location: 130.000 km

| SI No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.389 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.713 | gm |
| 4 | Weight of sand bottle with sand | 6.691 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.460 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.231 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 848.966 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 10 | % |
| 14 | Dry Density of soil | 0.104 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|--------|----|
| container no.= | I/11 | |
| wt of empty container= | 13.78 | gm |
| wt of cont. + wet soil= | 76.35 | gm |
| wt of cont. + dry soil = | 70.564 | gm |
| water content of excavated soil= | 10 | % |

Location: 140.100 km

| SI No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.345 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.669 | gm |
| 4 | Weight of sand bottle with sand | 6.691 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.275 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.416 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 976.552 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 15 | % |
| 14 | Dry Density of soil | 0.156 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|-------|----|
| container no.= | I/16 | |
| wt of empty container= | 12.54 | gm |
| wt of cont. + wet soil= | 72.56 | gm |
| wt of cont. + dry soil = | 64.52 | gm |
| water content of excavated soil= | 15 | % |

Location: 150.000 km

| Sl No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.389 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.713 | gm |
| 4 | Weight of sand bottle with sand | 6.691 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.468 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.223 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.410 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.645 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 817.812 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 13 | % |
| 14 | Dry Density of soil | 0.129 | gm/cc |

| 13. Water Content of excavated soil | | |
|-------------------------------------|--------|----|
| container no.= | I/23 | |
| wt of empty container= | 13.65 | gm |
| wt of cont. + wet soil= | 62.54 | gm |
| wt of cont. + dry soil = | 57.025 | gm |
| water content of excavated soil= | 13 | % |

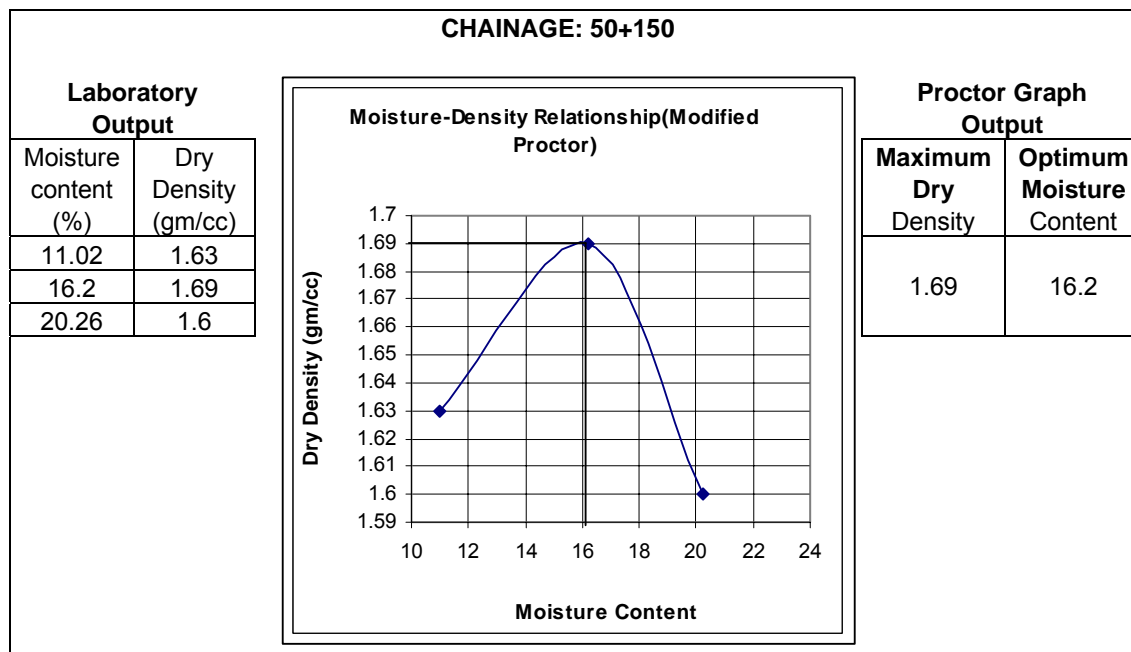
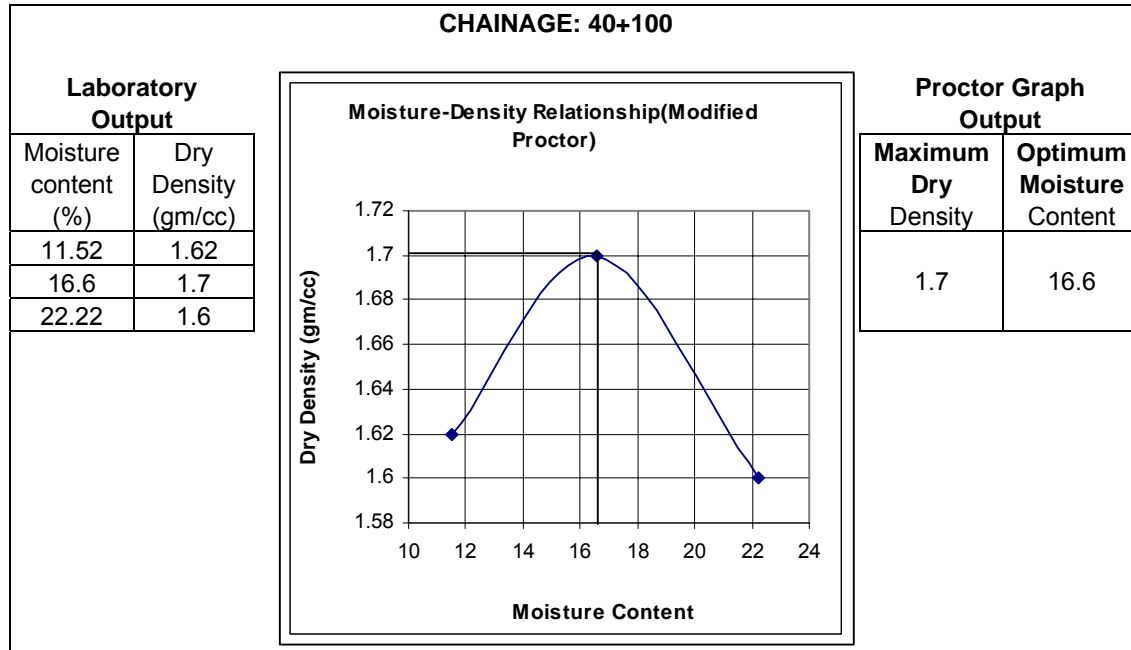
Location: 160.000 km

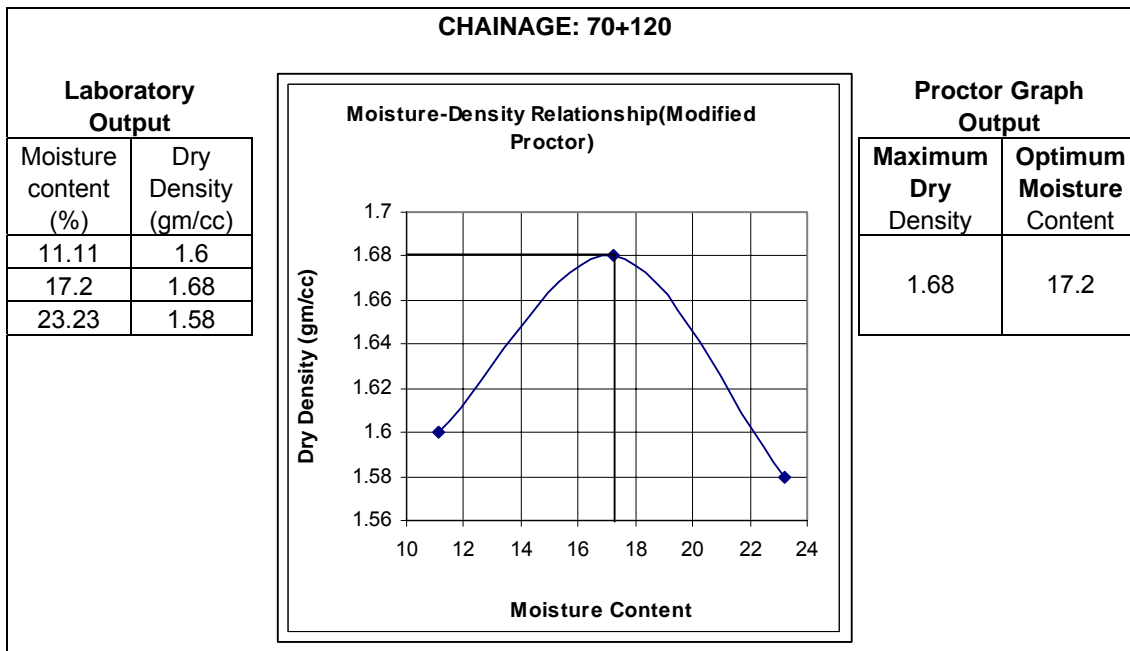
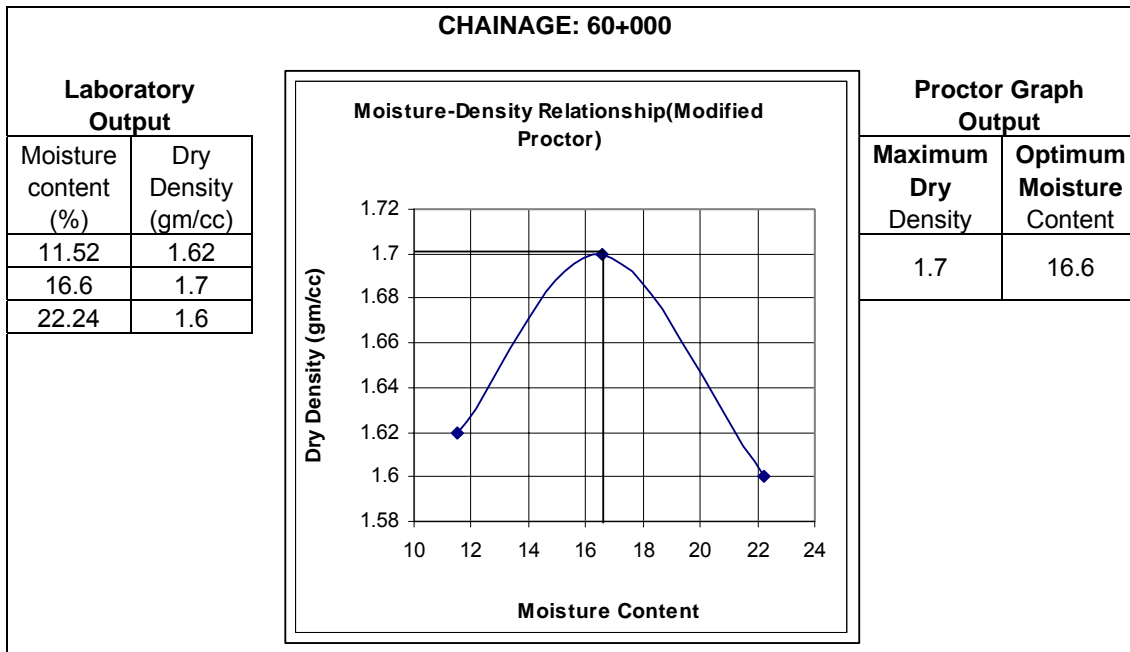
| SI No | Particulars | Quantity | Unit |
|-------|--|----------|-----------------|
| 1 | Weight of Pan + Soil (excavated) | 3.350 | gm |
| 2 | Weight of empty Pan | 1.676 | gm |
| 3 | Weight of excavated Soil (1-2) | 1.564 | gm |
| 4 | Weight of sand bottle with sand | 6.589 | gm |
| 5 | Weight of sand bottle after pouring the sand in to the pit | 5.373 | gm |
| 6 | Weight of sand required for filling the pit (4-5) | 1.216 | gm |
| 7 | Weight of graduated jar | 1.765 | gm |
| 8 | Weight of graduated jar full with sand (up to 1100 cc) | 3.360 | gm |
| 9 | Weight of 1100 cc sand (8-7) | 1.595 | gm |
| 10 | Bulk Density of Sand= (9)/1100 cc | 0.001 | gm/cc |
| 11 | Volume of Pit= (6)/(10) | 838.621 | cm ³ |
| 12 | Bulk Density of excavated soil= (3)/(11) | 0.002 | gm/cc |
| 13 | Water Content of excavated soil | 10 | % |
| 14 | Dry Density of soil | 0.106 | gm/cc |

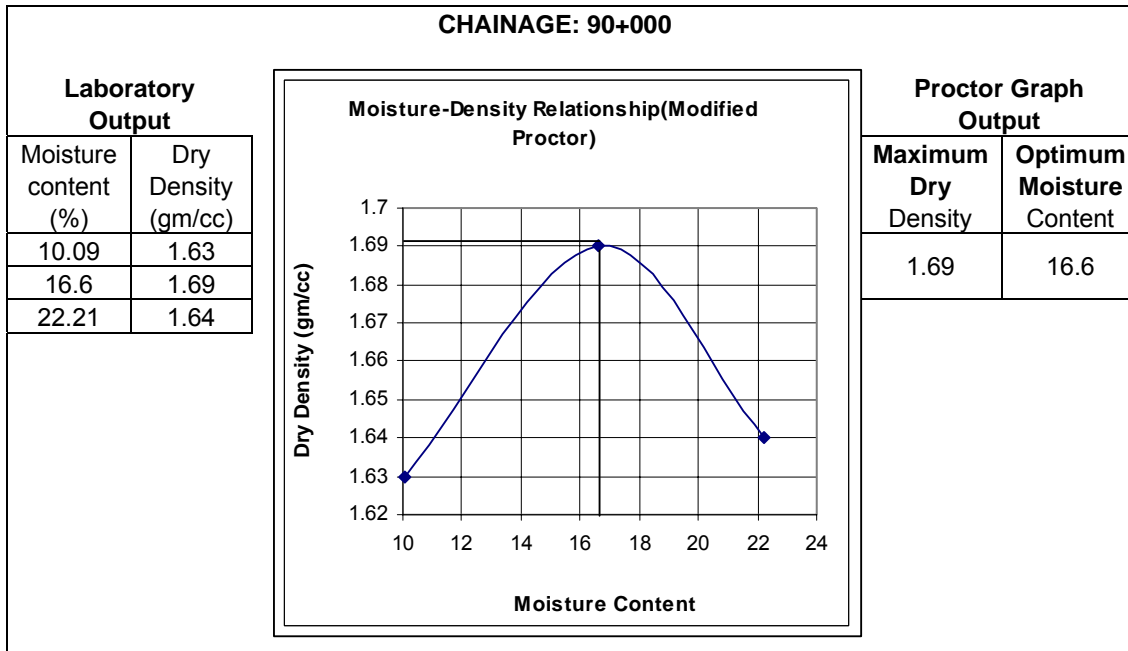
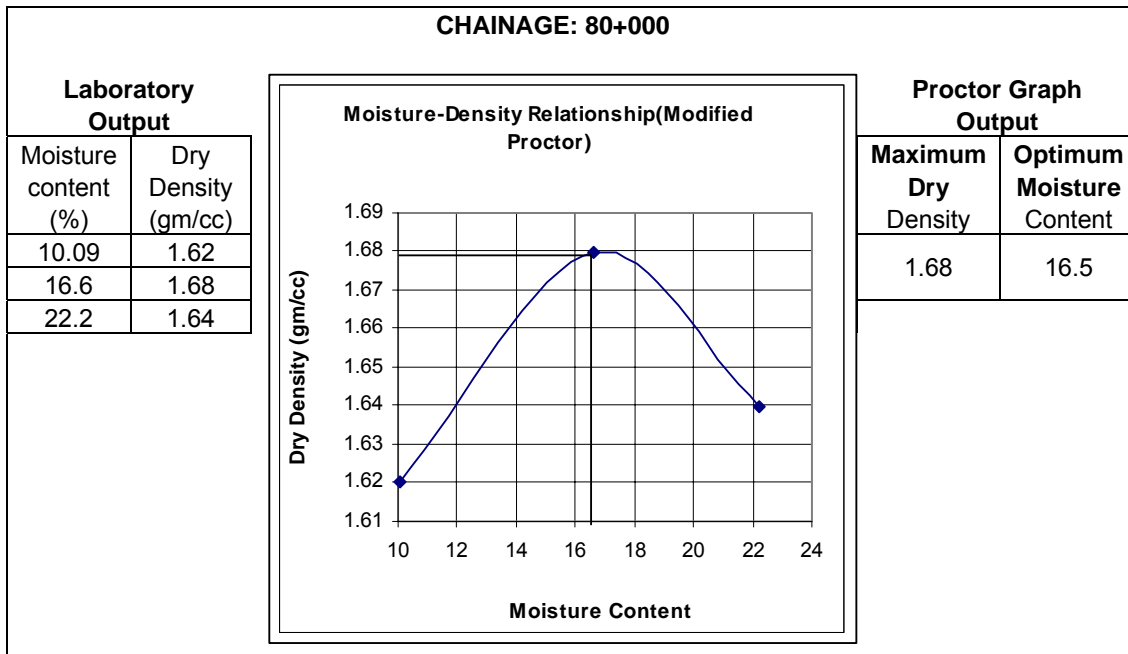
| 13. Water Content of excavated soil | | |
|-------------------------------------|---------|----|
| container no.= | 108 | |
| wt of empty container= | 23.56 | gm |
| wt of cont. + wet soil= | 125.63 | gm |
| wt of cont. + dry soil = | 116.025 | gm |
| water content of excavated soil= | 10 | % |

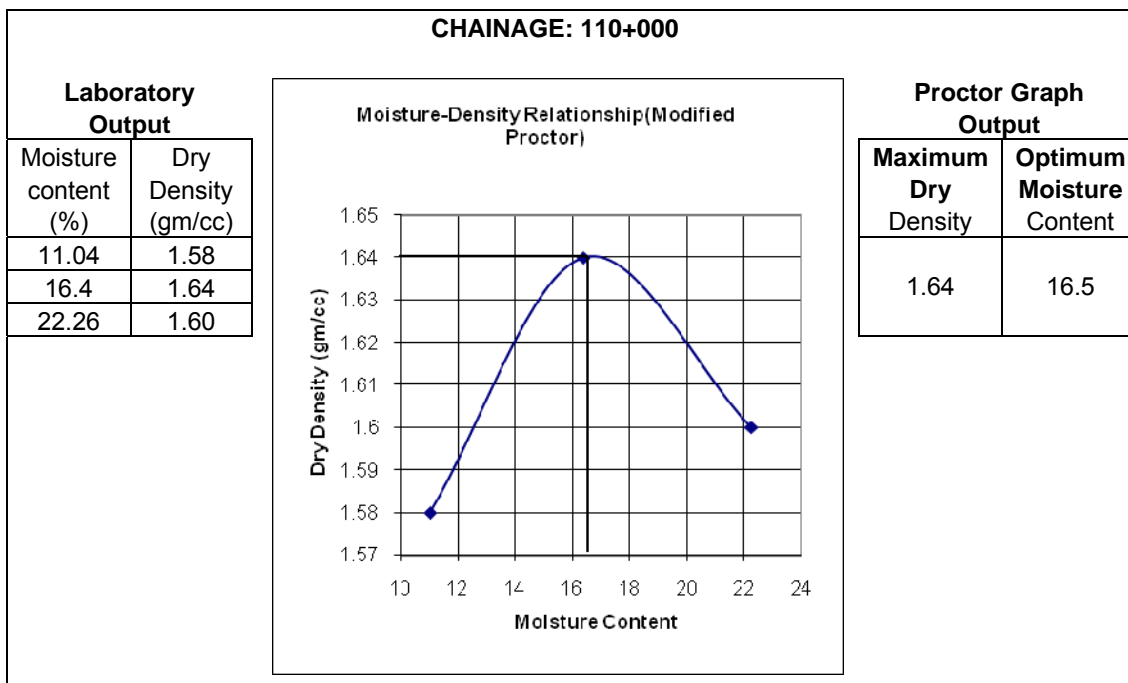
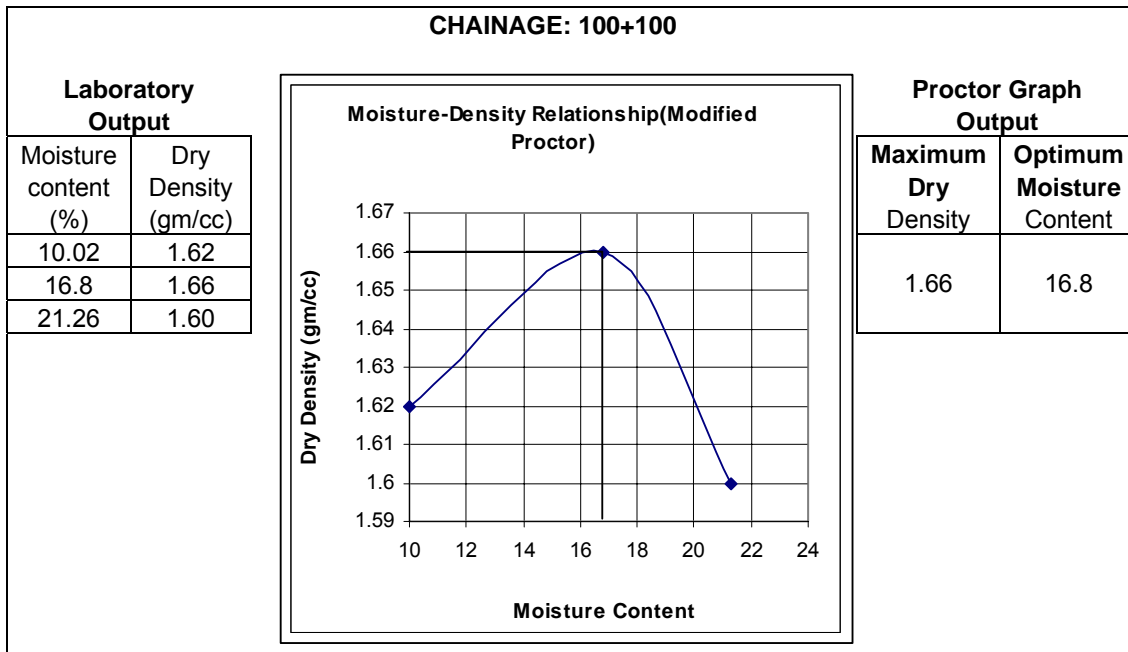
5. MODIFIED PROCTOR TEST

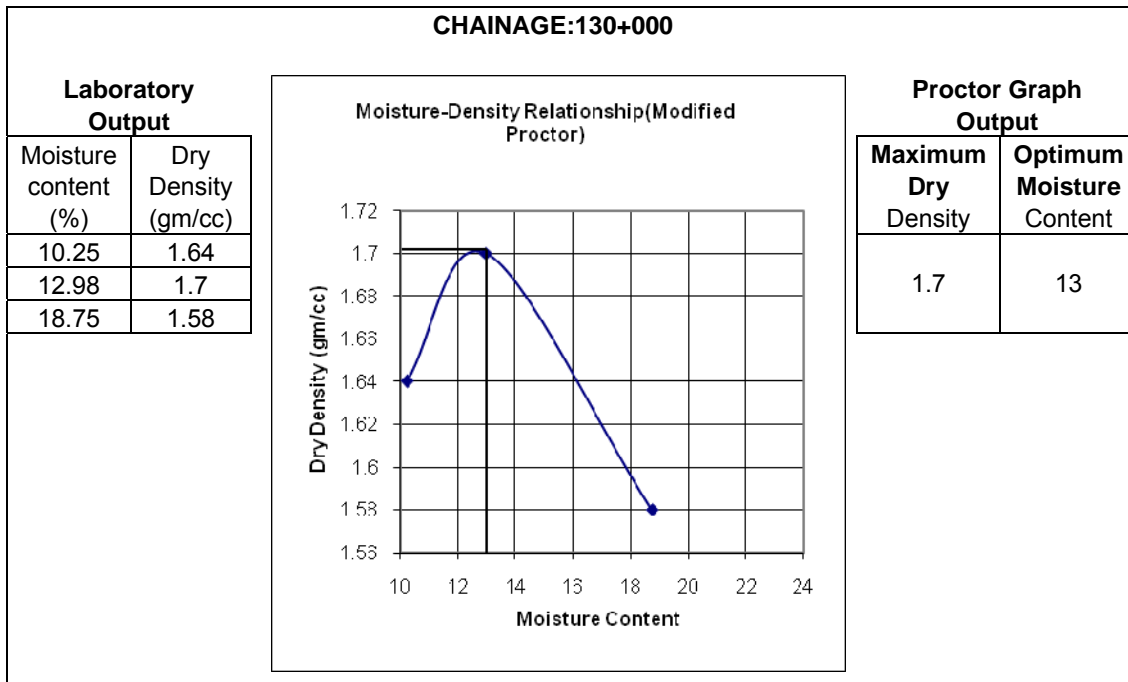
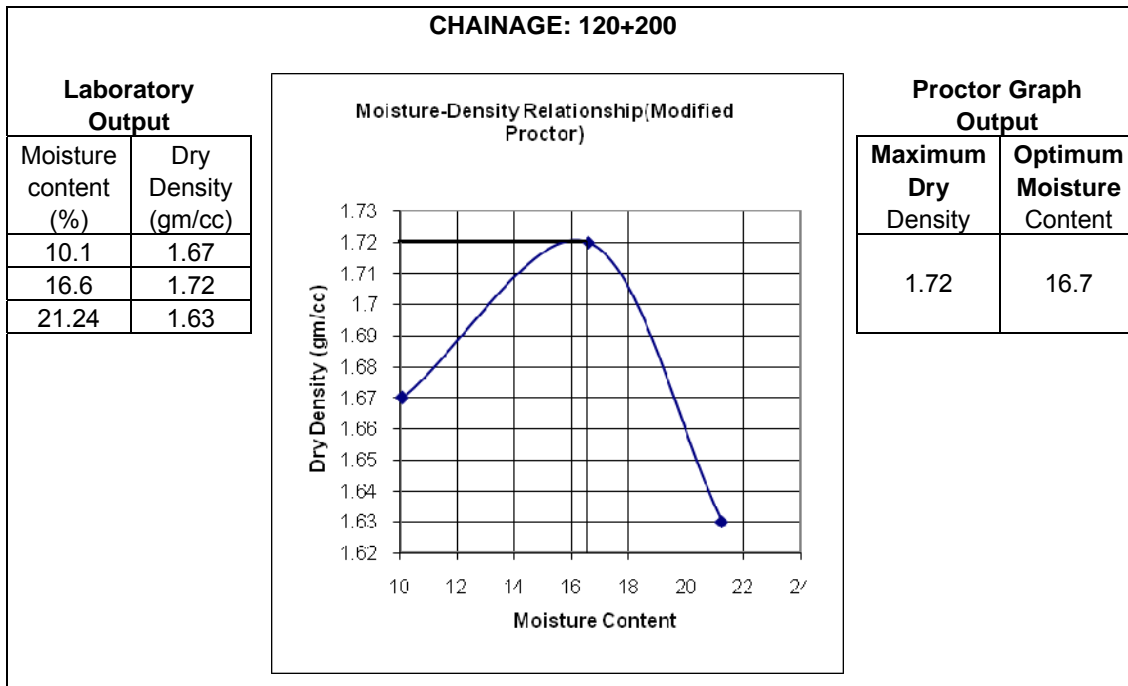
Modified proctor test gives the higher degree of compaction. In this test the soil is compacted in Standard Proctor Mould in 5 layers being given 25 blows of 4.5kg rammer dropped from a height of 450mm. This test determine the maximum Dry Density of the soil and corresponding optimum moisture content. Some Laboratory test results are given below.

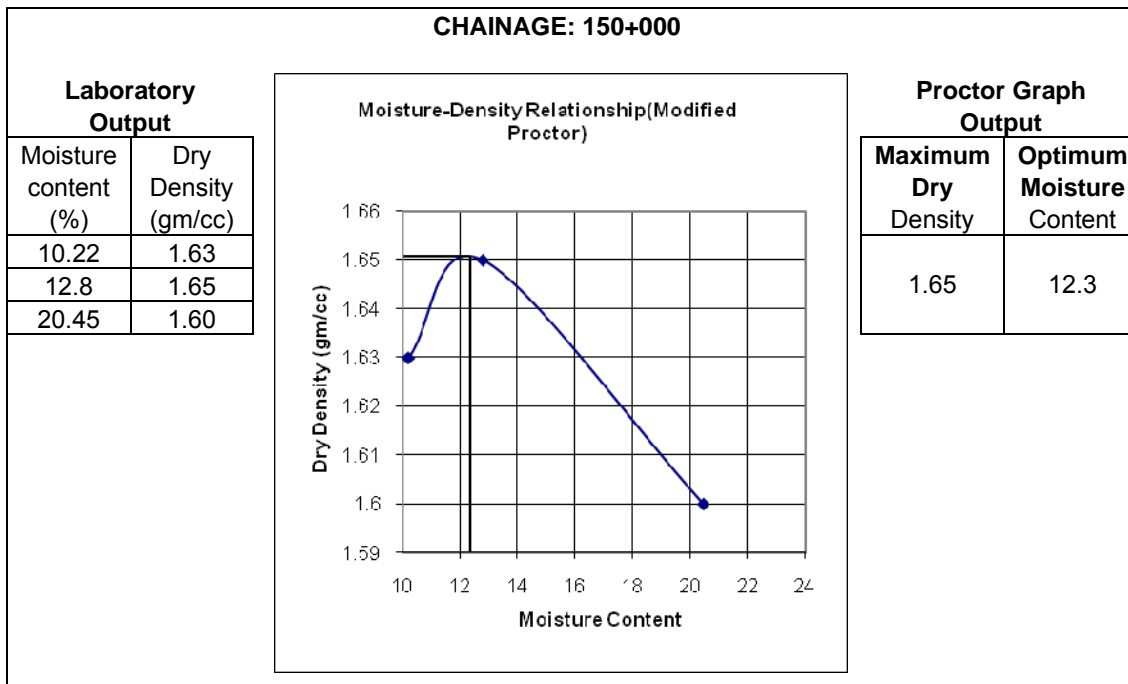
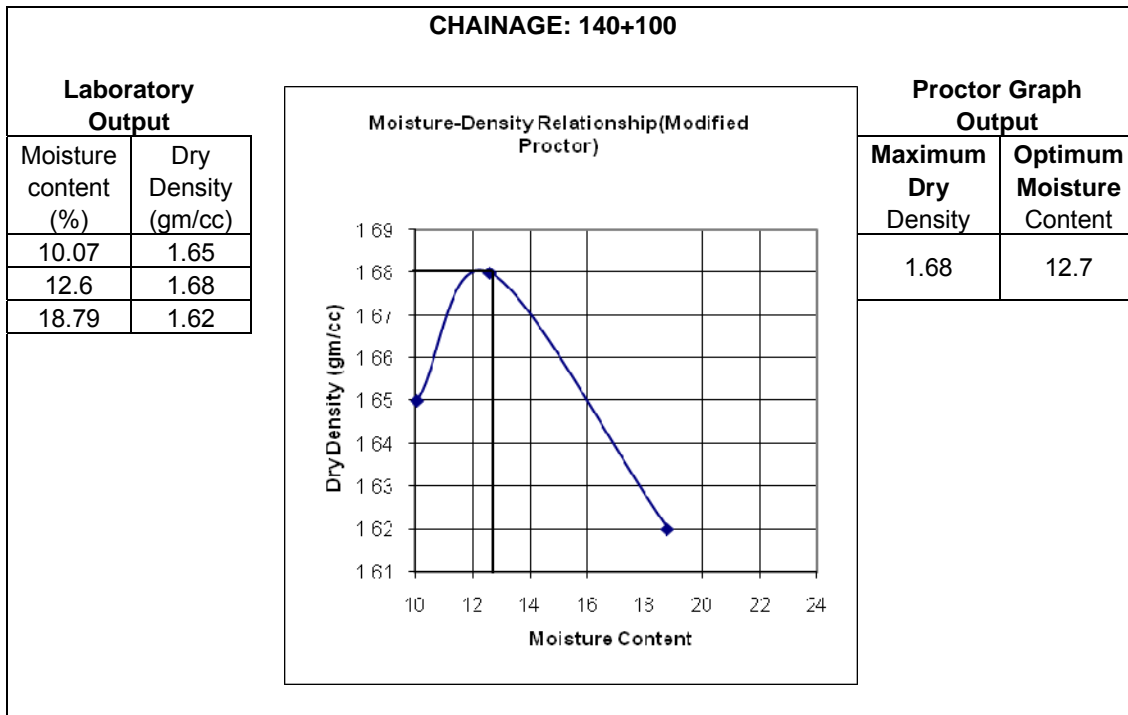


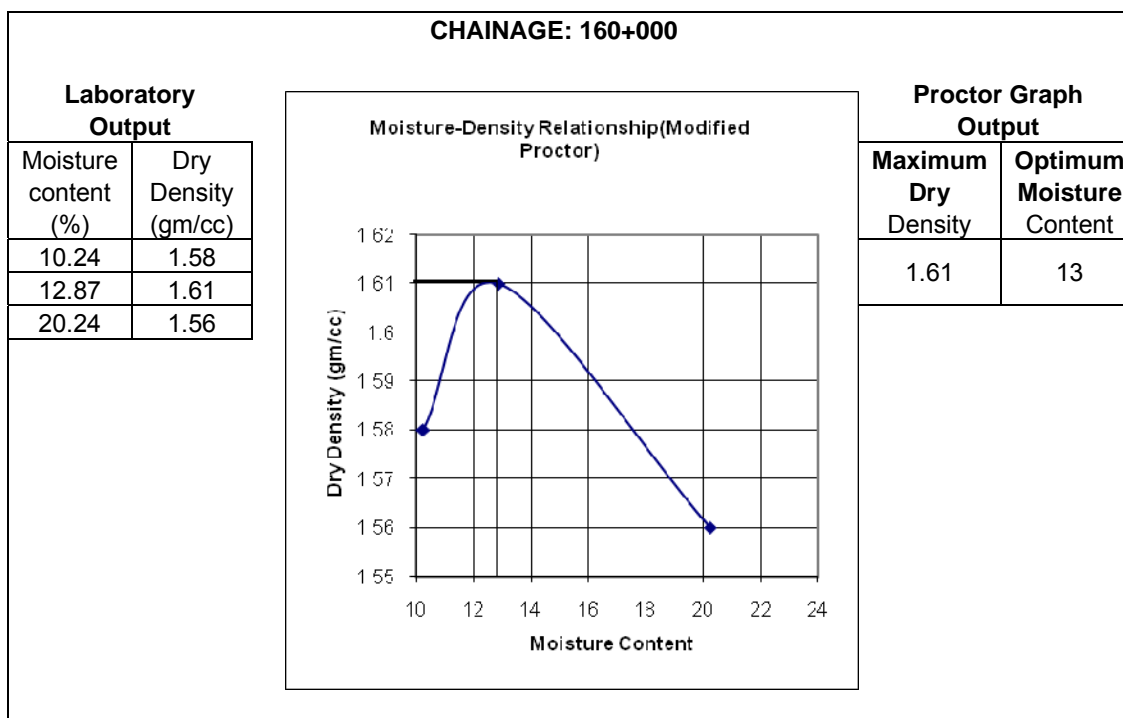












6. CALIFORNIA BEARING RATION TEST

California Bearing Ratio Test were performed on bulk samples collected from pavement subgrade of existing highway, from new alignment of widening portion and on borrow materials. The CBR was determined for 3 energy level on both unsoaked and 4 day soaked conditions. To achieve the required CBR of 7, the compaction criteria to be required were also studied. The results of different CBR test are shown in below.

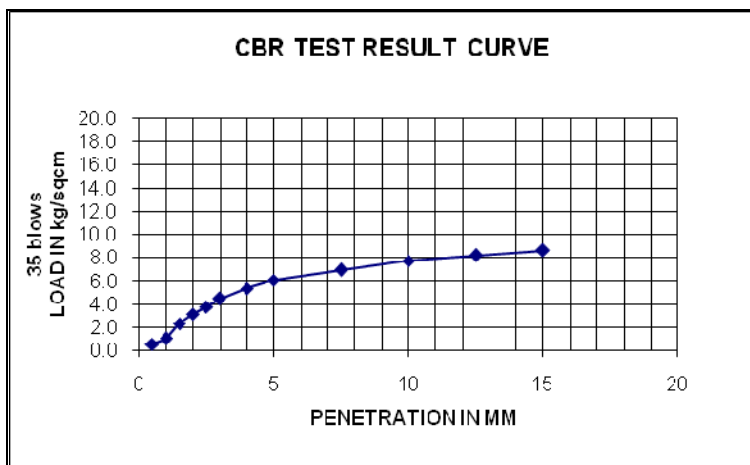
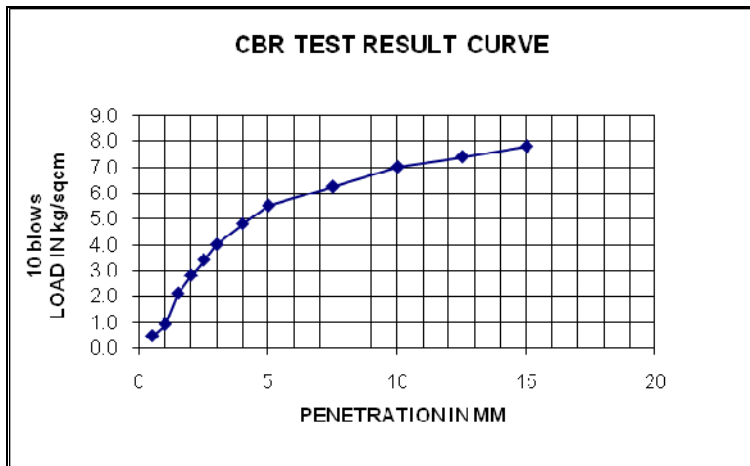
LOCATION: 40+100 km

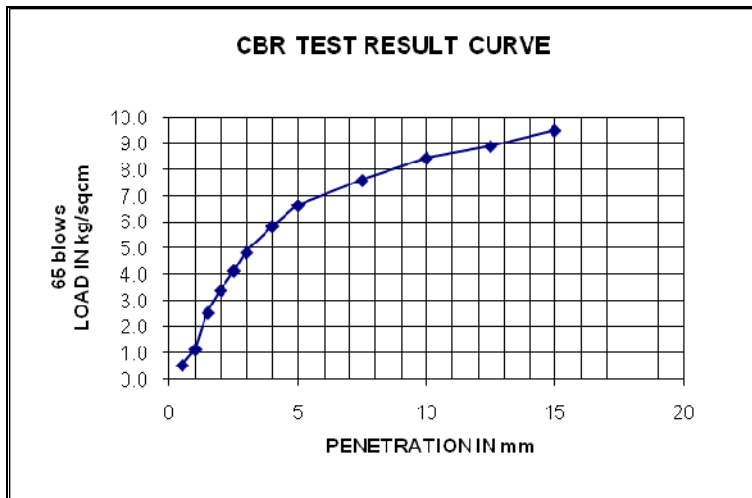
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

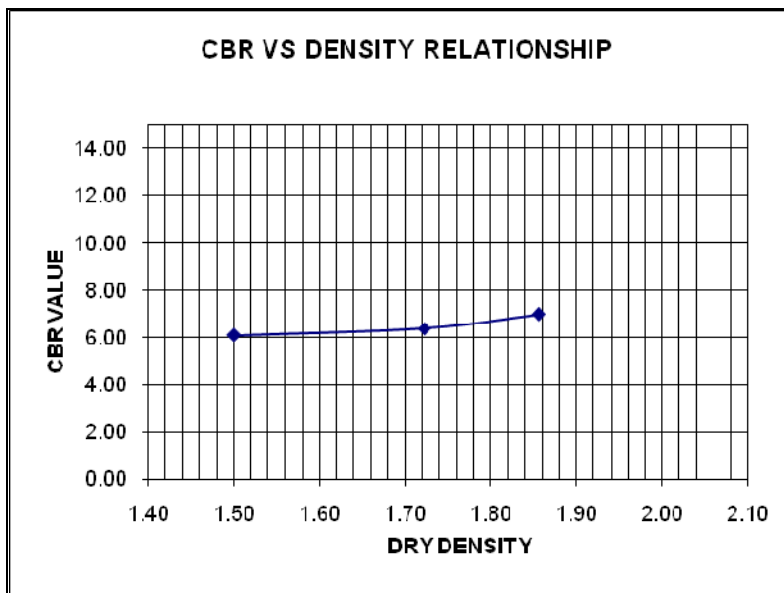
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9282 | 9854 | 10192 | 9728 | 10300 | 10643 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 3942 | 4514 | 4852 | 4388 | 4960 | 5303 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.75 | 2.01 | 2.16 | 1.95 | 2.20 | 2.36 |
| Water Content (%) | 16.8 | 16.5 | 16.2 | 30 | 28 | 27 |
| Dry Density (gms/cc) | 1.50 | 1.72 | 1.86 | 1.50 | 1.72 | 1.86 |

| Penetration (mm) | Penetration Data | | | | | | Standard Load kg/cm ² | Proving Ring Used: 1000kg | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| | TEST LOAD | | | | | | | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 9 | 10 | 11 | 0.5 | 0.5 | 0.6 | | | | | | | |
| 1.0 | 18 | 20 | 23 | 0.9 | 1.0 | 1.2 | | | | | | | |
| 1.5 | 42 | 46 | 51 | 2.1 | 2.3 | 2.6 | | | | | | | |
| 2.0 | 56 | 62 | 68 | 2.8 | 3.1 | 3.4 | | | | | | | |
| 2.5 | 68 | 75 | 83 | 3.4 | 3.8 | 4.2 | 70 | 4.0 | 4.4 | 4.8 | 5.7 | 6.3 | 6.9 |
| 3.0 | 80 | 88 | 97 | 4.0 | 4.4 | 4.9 | | | | | | | |
| 4.0 | 96 | 106 | 117 | 4.8 | 5.3 | 5.9 | | | | | | | |
| 5.0 | 110 | 121 | 133 | 5.5 | 6.1 | 6.7 | 105 | 6.4 | 6.7 | 7.3 | 6.1 | 6.4 | 7.0 |
| 7.5 | 125 | 138 | 152 | 6.3 | 6.9 | 7.6 | | | | | | | |
| 10.0 | 140 | 154 | 169 | 7.0 | 7.7 | 8.5 | | | | | | | |
| 12.5 | 148 | 163 | 178 | 7.4 | 8.2 | 8.9 | | | | | | | |
| 15.0 | 156 | 172 | 190 | 7.8 | 8.6 | 9.5 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 5.71 | 6.29 | 6.86 |
| 5 | 6.10 | 6.38 | 7.0 |



MDD=1.70 gm/cc; 97% of MDD=1.65 gm/cc
The CBR value to be adopted=CBR value of 97% of MDD=6.30 (from graph)

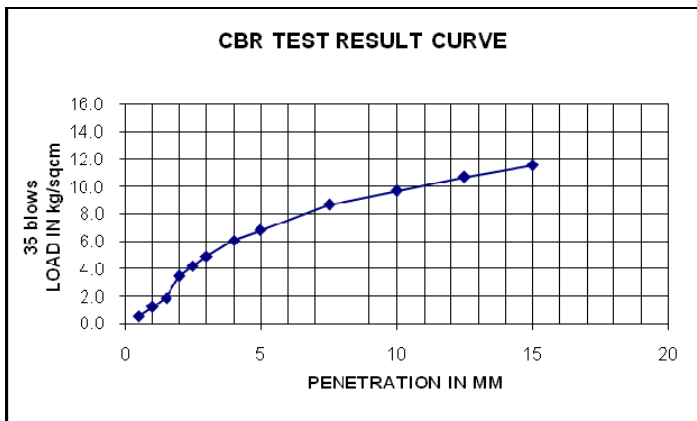
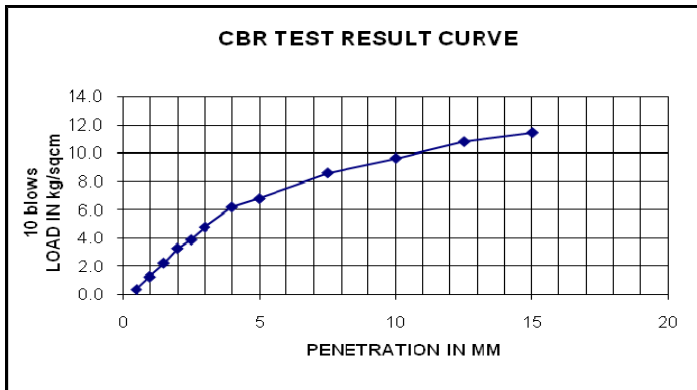
LOCATION: 50+150 km

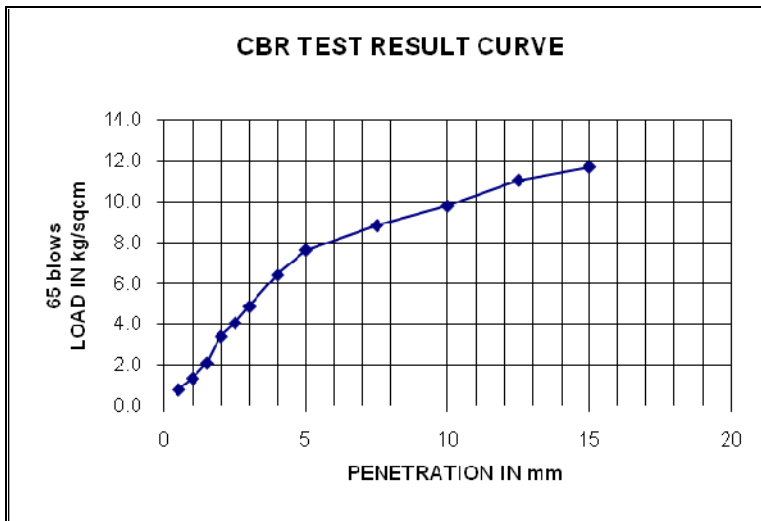
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

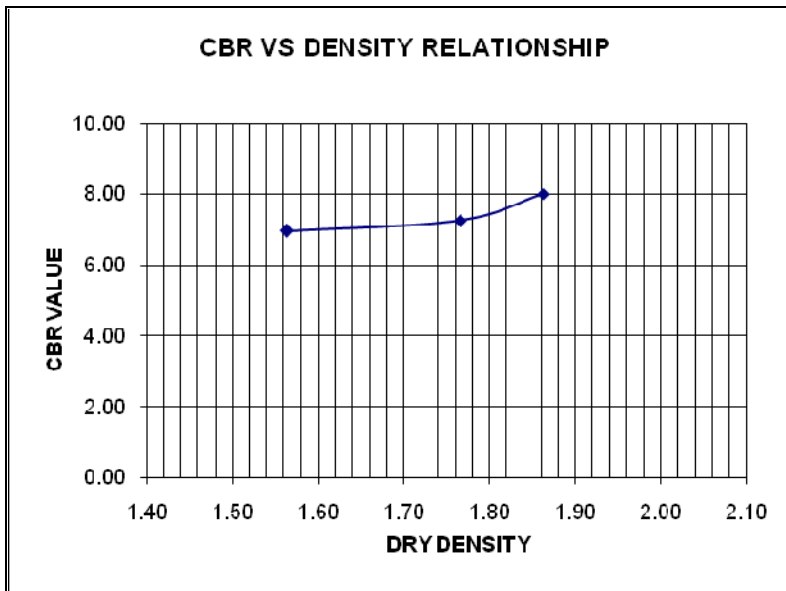
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9476 | 9989 | 10265 | 10088 | 10585 | 10831 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4136 | 4649 | 4925 | 4748 | 5245 | 5491 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.84 | 2.07 | 2.19 | 2.11 | 2.33 | 2.44 |
| Water Content (%) | 17.6 | 17 | 17.5 | 35 | 32 | 31 |
| Dry Density (gms/cc) | 1.56 | 1.77 | 1.86 | 1.56 | 1.77 | 1.86 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| | 0.5 | 8 | 12 | 16 | 0.4 | 0.6 | | 0.8 | | | | | |
| 1.0 | 26 | 25 | 27 | 1.3 | 1.3 | 1.4 | | | | | | | |
| 1.5 | 45 | 38 | 42 | 2.3 | 1.9 | 2.1 | | | | | | | |
| 2.0 | 66 | 70 | 68 | 3.3 | 3.5 | 3.4 | | | | | | | |
| 2.5 | 78 | 85 | 81 | 3.9 | 4.3 | 4.1 | 70 | 4.4 | 5.0 | 4.9 | 6.3 | 7.1 | 7.0 |
| 3.0 | 96 | 99 | 97 | 4.8 | 5.0 | 4.9 | | | | | | | |
| 4.0 | 124 | 122 | 128 | 6.2 | 6.1 | 6.4 | | | | | | | |
| 5.0 | 136 | 137 | 152 | 6.8 | 6.9 | 7.6 | 105 | 7.3 | 7.6 | 8.4 | 7.0 | 7.2 | 8.0 |
| 7.5 | 172 | 174 | 176 | 8.6 | 8.7 | 8.8 | | | | | | | |
| 10.0 | 193 | 194 | 195 | 9.7 | 9.7 | 9.8 | | | | | | | |
| 12.5 | 216 | 214 | 220 | 10.8 | 10.7 | 11.0 | | | | | | | |
| 15.0 | 229 | 231 | 233 | 11.5 | 11.6 | 11.7 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 6.29 | 7.14 | 7.00 |
| 5 | 6.95 | 7.24 | 8.00 |



MDD=1.72 gm/cc; 97% of MDD=1.67 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=7.00 (from graph)

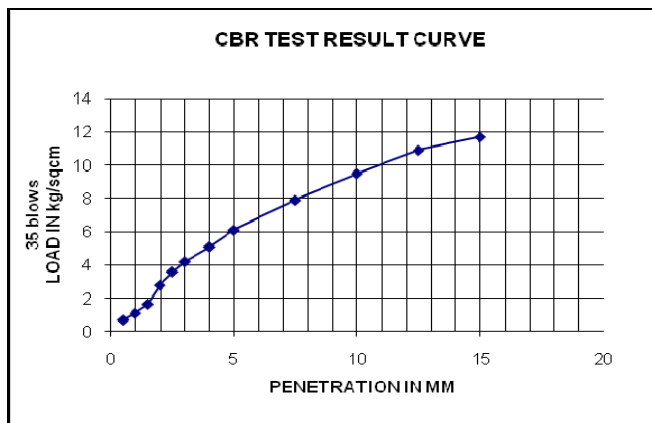
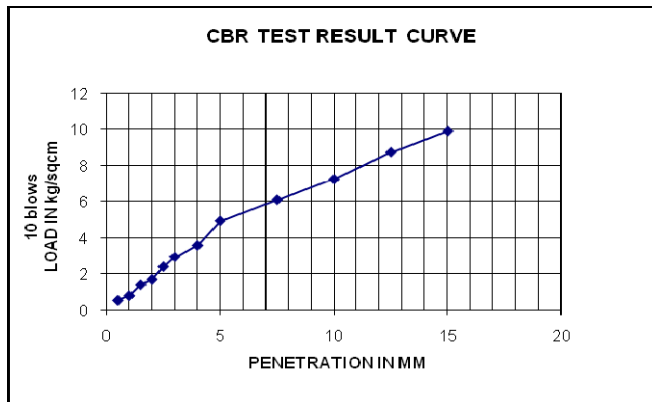
LOCATION: 60+000 km

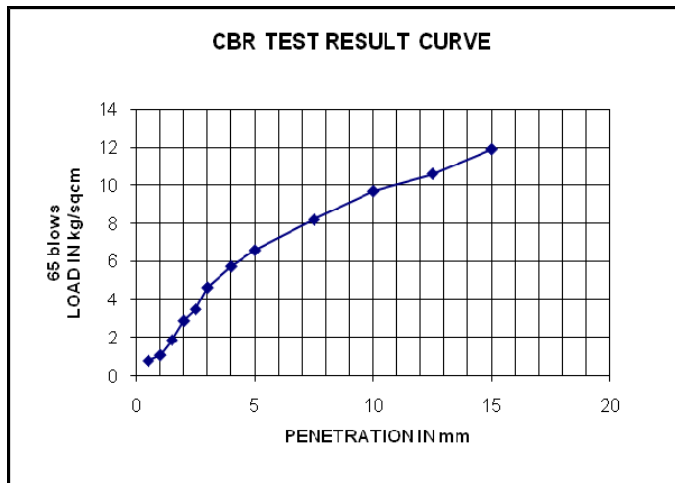
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

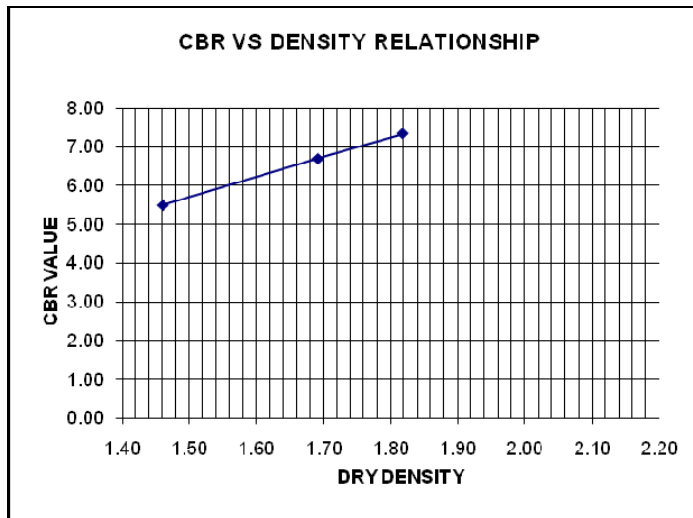
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9173 | 9785 | 10098 | 9613 | 10211 | 10495 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 3833 | 4445 | 4758 | 4273 | 4871 | 5155 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.70 | 1.98 | 2.11 | 1.90 | 2.16 | 2.29 |
| Water Content (%) | 16.6 | 16.8 | 16.3 | 30 | 28 | 26 |
| Dry Density (gms/cc) | 1.46 | 1.69 | 1.82 | 1.46 | 1.69 | 1.82 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|------|------|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| | 0.5 | 11 | 14 | 16 | 0.55 | 0.7 | | 0.8 | | | | | |
| 1.0 | 16 | 22 | 22 | 0.8 | 1.1 | 1.1 | | | | | | | |
| 1.5 | 28 | 33 | 38 | 1.4 | 1.65 | 1.9 | | | | | | | |
| 2.0 | 34 | 56 | 58 | 1.7 | 2.8 | 2.9 | | | | | | | |
| 2.5 | 48 | 72 | 70 | 2.4 | 3.6 | 3.5 | 70 | 3.2 | 4.5 | 4.6 | 4.57 | 6.43 | 6.57 |
| 3.0 | 59 | 84 | 93 | 2.95 | 4.2 | 4.65 | | | | | | | |
| 4.0 | 72 | 102 | 115 | 3.6 | 5.1 | 5.75 | | | | | | | |
| 5.0 | 99 | 122 | 132 | 4.95 | 6.1 | 6.6 | 105 | 5.75 | 7.0 | 7.7 | 5.48 | 6.67 | 7.33 |
| 7.5 | 122 | 158 | 164 | 6.1 | 7.9 | 8.2 | | | | | | | |
| 10.0 | 145 | 190 | 194 | 7.25 | 9.5 | 9.7 | | | | | | | |
| 12.5 | 175 | 218 | 212 | 8.75 | 10.9 | 10.6 | | | | | | | |
| 15.0 | 198 | 234 | 238 | 9.9 | 11.7 | 11.9 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 4.57 | 6.43 | 6.57 |
| 5 | 5.50 | 6.70 | 7.33 |



MDD=1.63 gm/cc; 97% of MDD=1.58 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=6.00 (from graph)

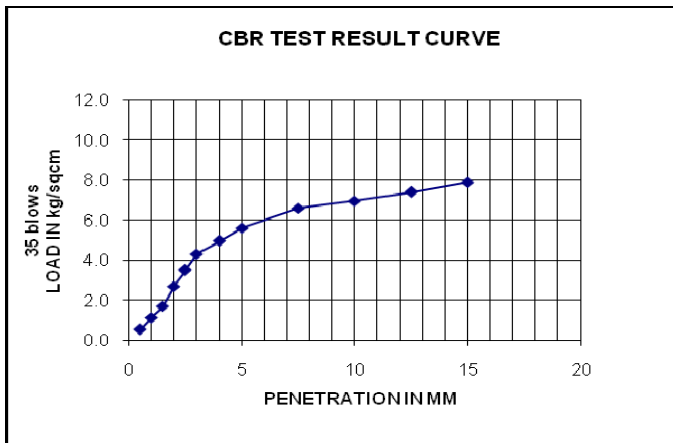
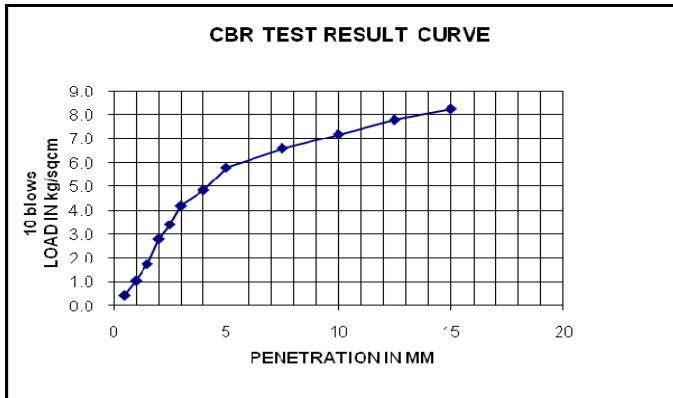
LOCATION: 70+120 km

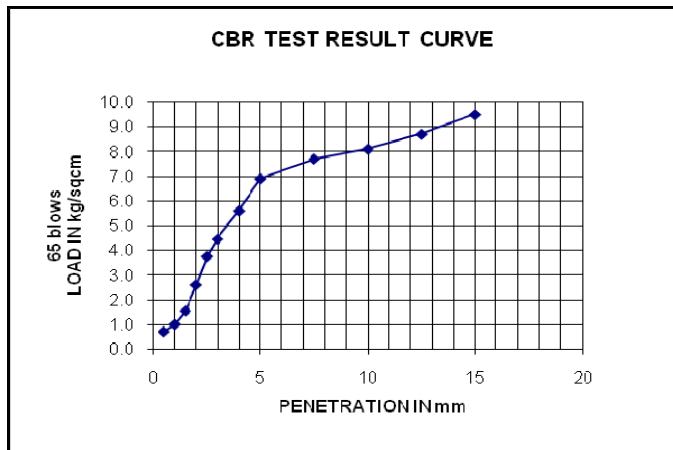
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

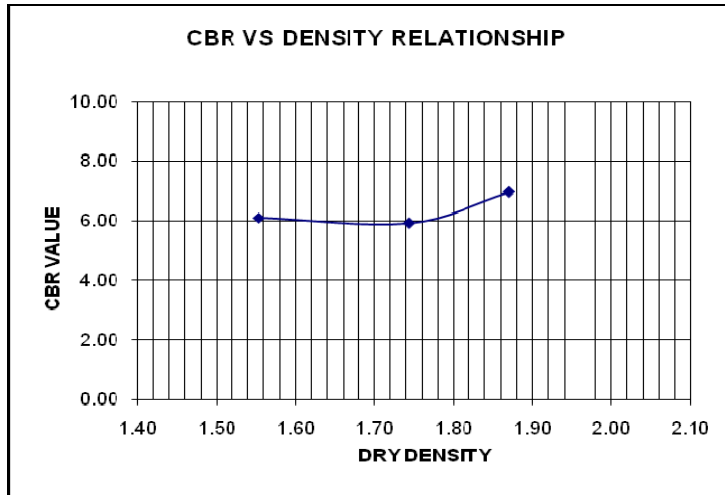
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9456 | 9948 | 10262 | 10127 | 10674 | 11019 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4116 | 4608 | 4922 | 4787 | 5334 | 5679 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.83 | 2.05 | 2.19 | 2.13 | 2.37 | 2.52 |
| Water Content (%) | 17.8 | 17.5 | 17 | 37 | 36 | 35 |
| Dry Density (gms/cc) | 1.55 | 1.74 | 1.87 | 1.55 | 1.74 | 1.87 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 9 | 11 | 14 | 0.5 | 0.6 | 0.7 | | | | | | | |
| 1.0 | 21 | 23 | 20 | 1.1 | 1.2 | 1.0 | | | | | | | |
| 1.5 | 35 | 34 | 31 | 1.8 | 1.7 | 1.6 | | | | | | | |
| 2.0 | 56 | 54 | 52 | 2.8 | 2.7 | 2.6 | | | | | | | |
| 2.5 | 68 | 70 | 75 | 3.4 | 3.5 | 3.8 | 70 | 4.0 | 4.1 | 4.2 | 5.7 | 5.9 | 6.0 |
| 3.0 | 84 | 86 | 89 | 4.2 | 4.3 | 4.5 | | | | | | | |
| 4.0 | 97 | 99 | 112 | 4.9 | 5.0 | 5.6 | | | | | | | |
| 5.0 | 116 | 112 | 138 | 5.8 | 5.6 | 6.9 | 105 | 6.4 | 6.2 | 7.3 | 6.1 | 5.9 | 7.0 |
| 7.5 | 132 | 132 | 154 | 6.6 | 6.6 | 7.7 | | | | | | | |
| 10.0 | 144 | 139 | 162 | 7.2 | 7.0 | 8.1 | | | | | | | |
| 12.5 | 156 | 148 | 174 | 7.8 | 7.4 | 8.7 | | | | | | | |
| 15.0 | 165 | 158 | 190 | 8.3 | 7.9 | 9.5 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 5.71 | 5.86 | 6.00 |
| 5 | 6.10 | 5.90 | 7.0 |



MDD=1.70 gm/cc; 97% of MDD=1.65 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=5.90 (from graph)

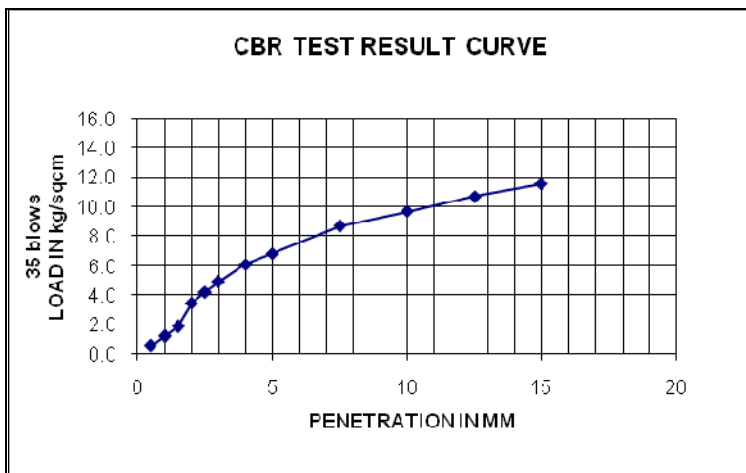
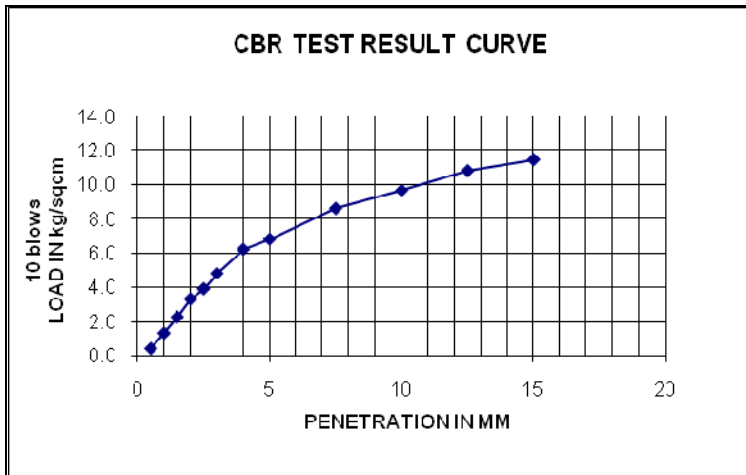
LOCATION: 80+000 km

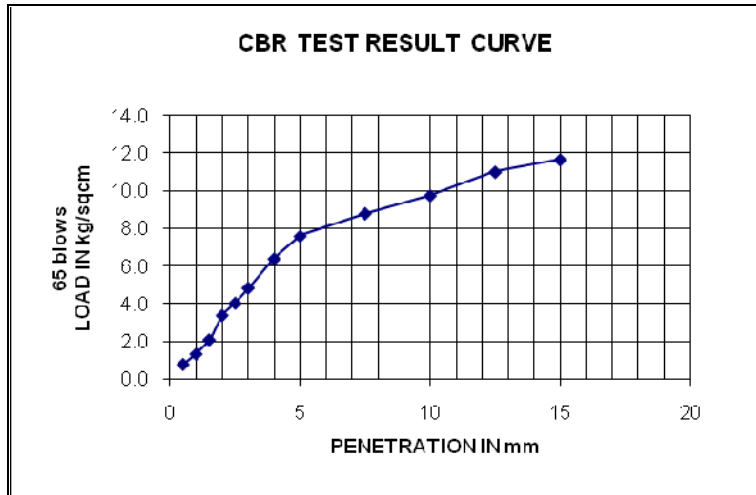
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

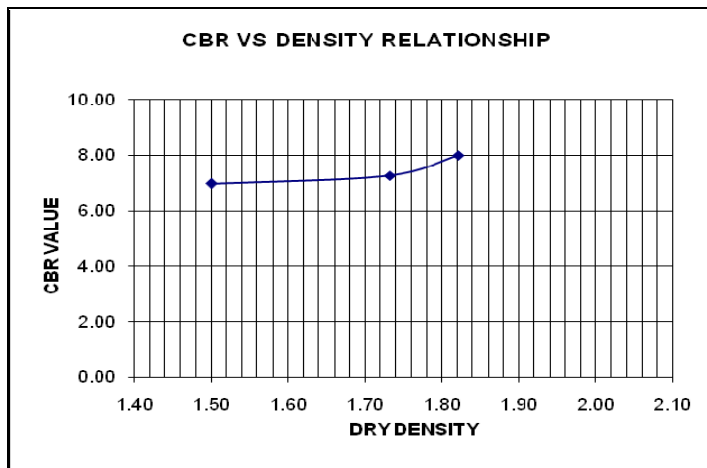
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9365 | 9982 | 10212 | 9827 | 10407 | 10544 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4025 | 4642 | 4872 | 4487 | 5067 | 5204 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.79 | 2.06 | 2.17 | 1.99 | 2.25 | 2.31 |
| Water Content (%) | 19.3 | 19.1 | 18.9 | 33 | 30 | 27 |
| Dry Density (gms/cc) | 1.50 | 1.73 | 1.82 | 1.50 | 1.73 | 1.82 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 8 | 12 | 16 | 0.4 | 0.6 | 0.8 | | | | | | | |
| 1.0 | 26 | 25 | 27 | 1.3 | 1.3 | 1.4 | | | | | | | |
| 1.5 | 45 | 38 | 42 | 2.3 | 1.9 | 2.1 | | | | | | | |
| 2.0 | 66 | 70 | 68 | 3.3 | 3.5 | 3.4 | | | | | | | |
| 2.5 | 78 | 85 | 81 | 3.9 | 4.3 | 4.1 | 70 | 4.4 | 5.0 | 4.9 | 6.3 | 7.1 | 7.0 |
| 3.0 | 96 | 99 | 97 | 4.8 | 5.0 | 4.9 | | | | | | | |
| 4.0 | 124 | 122 | 128 | 6.2 | 6.1 | 6.4 | | | | | | | |
| 5.0 | 136 | 137 | 152 | 6.8 | 6.9 | 7.6 | 105 | 7.3 | 7.6 | 8.4 | 7.0 | 7.2 | 8.0 |
| 7.5 | 172 | 174 | 176 | 8.6 | 8.7 | 8.8 | | | | | | | |
| 10.0 | 193 | 194 | 195 | 9.7 | 9.7 | 9.8 | | | | | | | |
| 12.5 | 216 | 214 | 220 | 10.8 | 10.7 | 11.0 | | | | | | | |
| 15.0 | 229 | 231 | 233 | 11.5 | 11.6 | 11.7 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 6.29 | 7.14 | 7.00 |
| 5 | 6.95 | 7.24 | 8.00 |



MDD=1.65 gm/cc; 97% of MDD=1.60 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=7.00 (from graph)

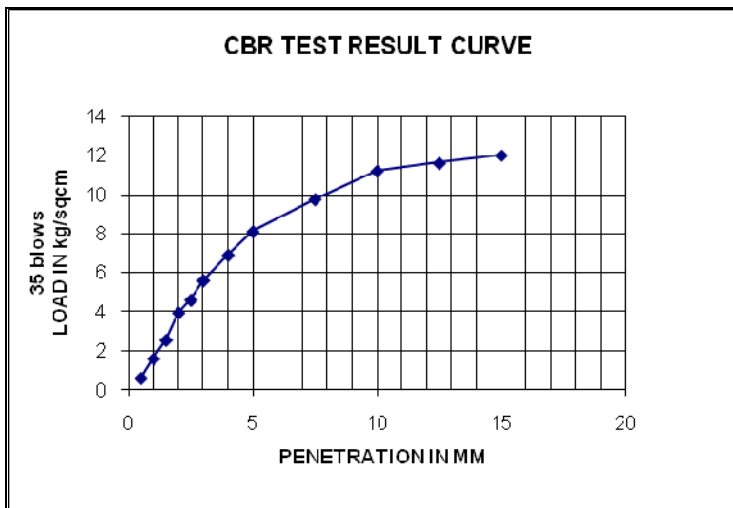
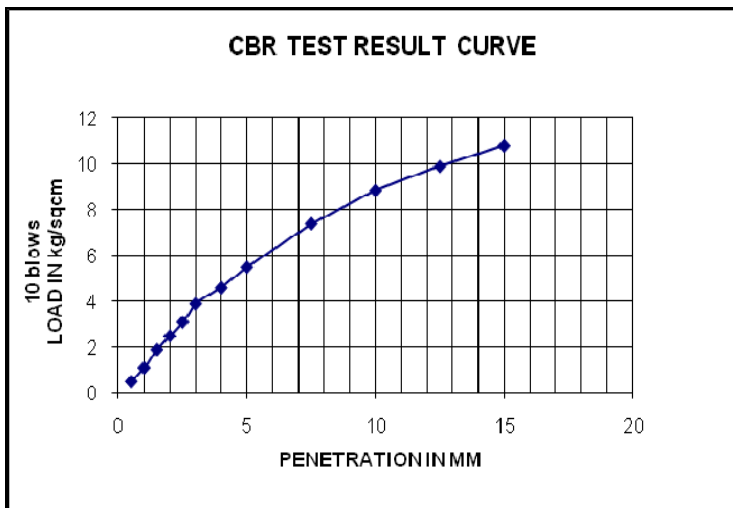
LOCATION: 90+000 km

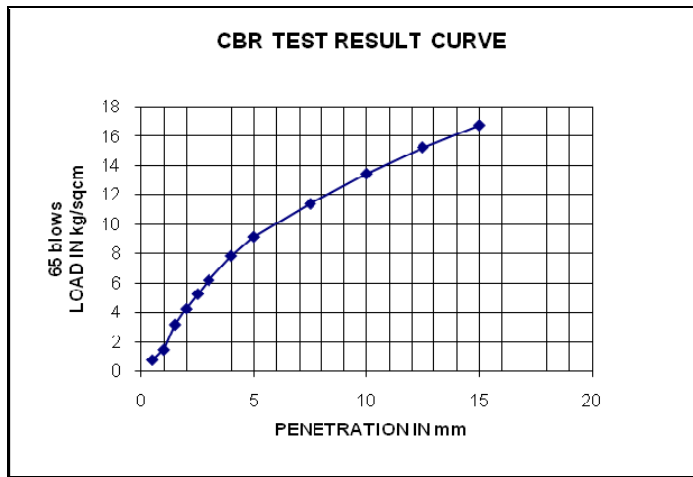
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

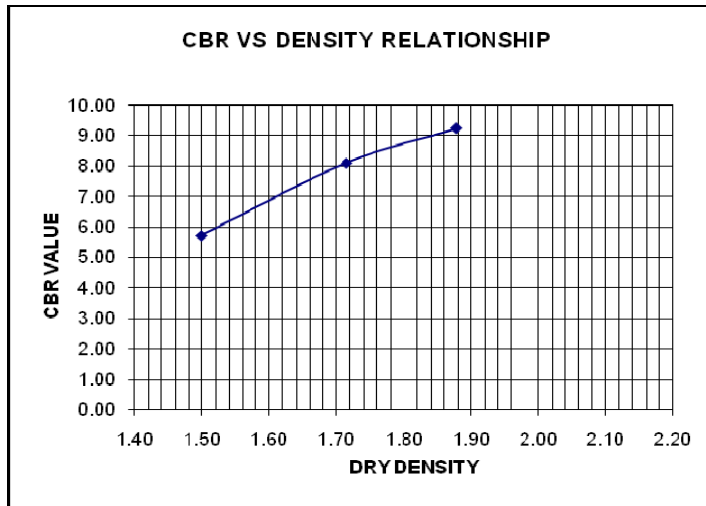
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9323 | 9921 | 10322 | 9792 | 10241 | 10622 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 3983 | 4581 | 4982 | 4452 | 4901 | 5282 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.77 | 2.04 | 2.21 | 1.98 | 2.18 | 2.35 |
| Water Content (%) | 18.1 | 18.7 | 17.9 | 32 | 27 | 25 |
| Dry Density (gms/cc) | 1.50 | 1.72 | 1.88 | 1.50 | 1.72 | 1.88 |

| Penetration (mm) | Penetration Data | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|-------------------------------------|--------------------------------------|-----|-----|--------------|------|------|
| | TEST LOAD | | | | | | Standard Load (kg/cm ²) | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 10 | 12 | 14 | 0.5 | 0.6 | 0.7 | | | | | | | |
| 1.0 | 22 | 32 | 28 | 1.1 | 1.6 | 1.4 | | | | | | | |
| 1.5 | 38 | 51 | 62 | 1.9 | 2.55 | 3.1 | | | | | | | |
| 2.0 | 50 | 79 | 84 | 2.5 | 3.95 | 4.2 | | | | | | | |
| 2.5 | 62 | 92 | 104 | 3.1 | 4.6 | 5.2 | 70 | 3.6 | 5 | 5.8 | 5.14 | 7.14 | 8.29 |
| 3.0 | 78 | 112 | 123 | 3.9 | 5.6 | 6.15 | | | | | | | |
| 4.0 | 92 | 138 | 156 | 4.6 | 6.9 | 7.8 | | | | | | | |
| 5.0 | 110 | 162 | 182 | 5.5 | 8.1 | 9.1 | 105 | 6.0 | 8.5 | 9.7 | 5.71 | 8.10 | 9.24 |
| 7.5 | 148 | 195 | 227 | 7.4 | 9.75 | 11.35 | | | | | | | |
| 10.0 | 177 | 224 | 268 | 8.85 | 11.2 | 13.4 | | | | | | | |
| 12.5 | 198 | 232 | 304 | 9.9 | 11.6 | 15.2 | | | | | | | |
| 15.0 | 216 | 240 | 334 | 10.8 | 12 | 16.7 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 5.14 | 7.14 | 8.29 |
| 5 | 5.71 | 8.10 | 9.24 |



MDD=1.65 gm/cc; 97% of MDD=1.60 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=7.00 (from graph)

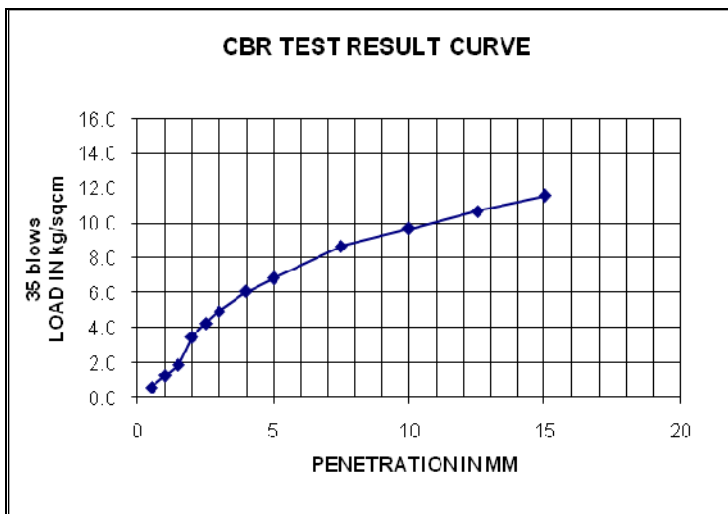
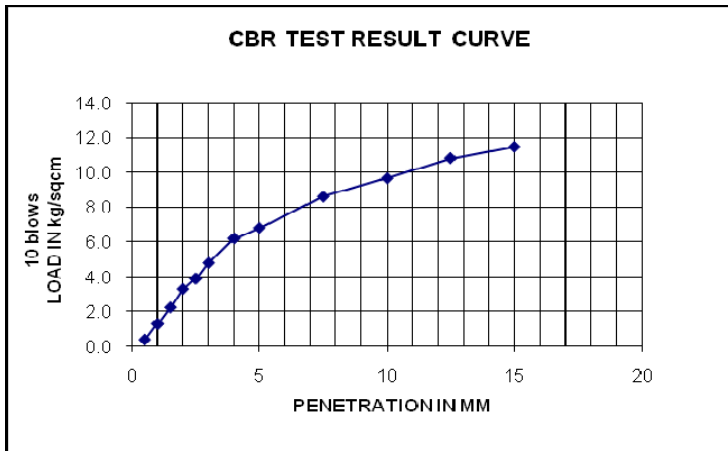
LOCATION: 100+100 km

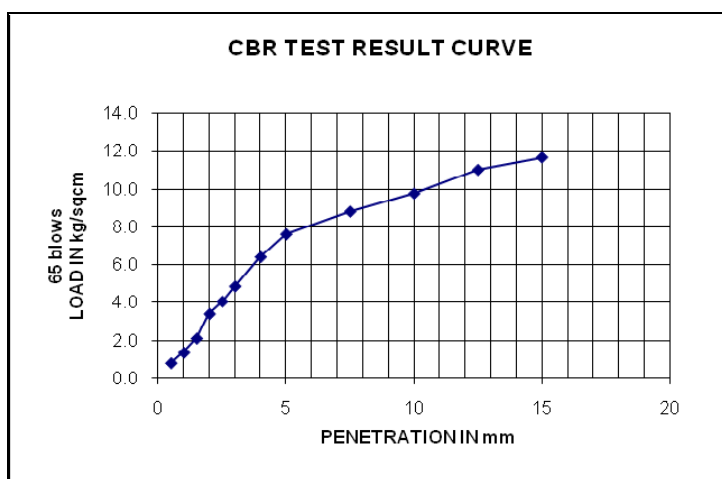
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

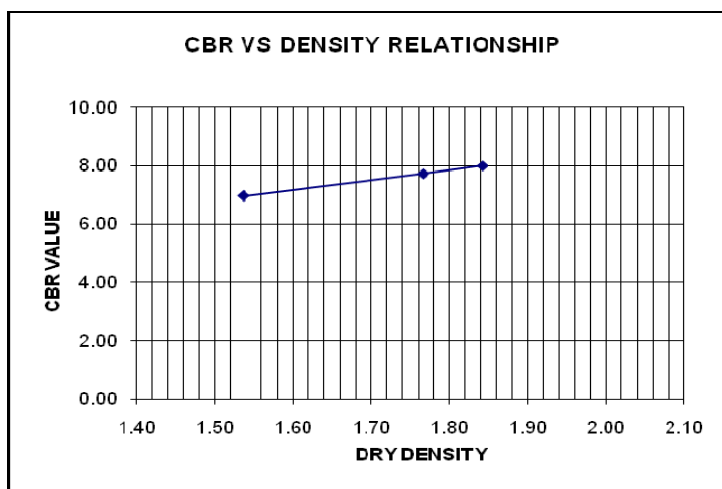
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9406 | 9990 | 10210 | 10008 | 10586 | 10645 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4066 | 4650 | 4870 | 4668 | 5246 | 5305 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.81 | 2.07 | 2.16 | 2.07 | 2.33 | 2.36 |
| Water Content (%) | 17.6 | 17 | 17.5 | 35 | 32 | 28 |
| Dry Density (gms/cc) | 1.54 | 1.77 | 1.84 | 1.54 | 1.77 | 1.84 |

| Penetration (mm) | Penetration Data | | | | | | Proving Ring Used: 1000kg | | | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|-------------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|--|--|
| | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 | | |
| 0.5 | 8 | 12 | 16 | 0.4 | 0.6 | 0.8 | | | | | | | | | |
| 1.0 | 26 | 25 | 27 | 1.3 | 1.3 | 1.4 | | | | | | | | | |
| 1.5 | 45 | 38 | 42 | 2.3 | 1.9 | 2.1 | | | | | | | | | |
| 2.0 | 66 | 70 | 68 | 3.3 | 3.5 | 3.4 | | | | | | | | | |
| 2.5 | 78 | 85 | 81 | 3.9 | 4.3 | 4.1 | 70 | 4.4 | 5.5 | 4.9 | 6.3 | 7.9 | 7.0 | | |
| 3.0 | 96 | 99 | 97 | 4.8 | 5.0 | 4.9 | | | | | | | | | |
| 4.0 | 124 | 122 | 128 | 6.2 | 6.1 | 6.4 | | | | | | | | | |
| 5.0 | 136 | 137 | 152 | 6.8 | 6.9 | 7.6 | 105 | 7.3 | 8.1 | 8.4 | 7.0 | 7.7 | 8.0 | | |
| 7.5 | 172 | 174 | 176 | 8.6 | 8.7 | 8.8 | | | | | | | | | |
| 10.0 | 193 | 194 | 195 | 9.7 | 9.7 | 9.8 | | | | | | | | | |
| 12.5 | 216 | 214 | 220 | 10.8 | 10.7 | 11.0 | | | | | | | | | |
| 15.0 | 229 | 231 | 233 | 11.5 | 11.6 | 11.7 | | | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 6.29 | 7.86 | 7.00 |
| 5 | 6.95 | 7.71 | 8.00 |



MDD=1.71 gm/cc; 97% of MDD=1.66 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=7.00 (from graph)

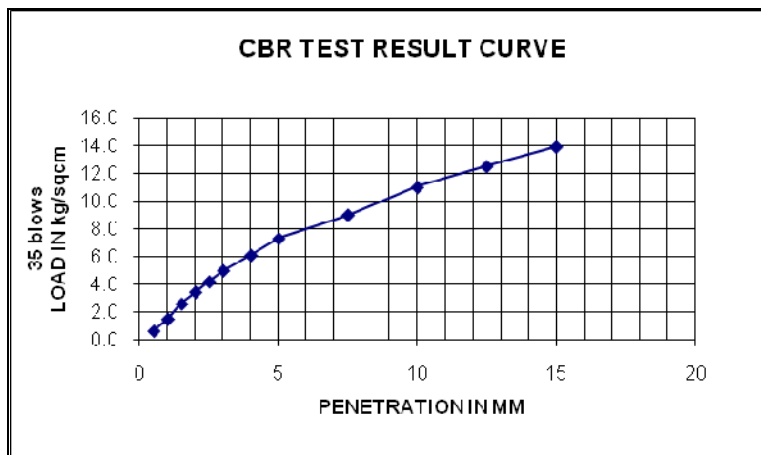
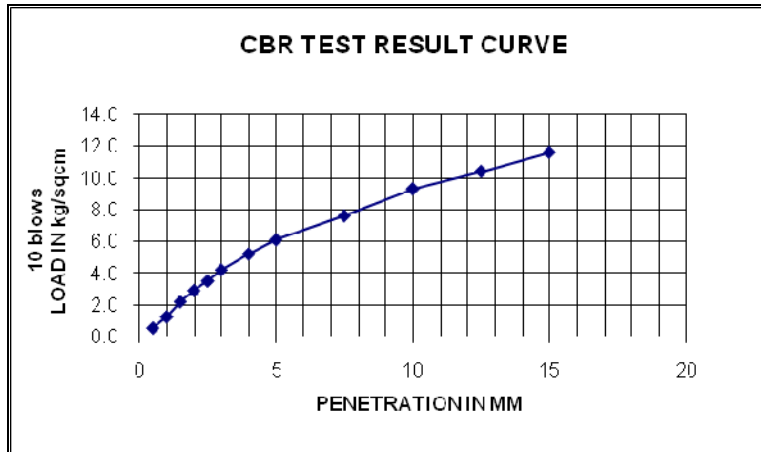
LOCATION: 110+000 km

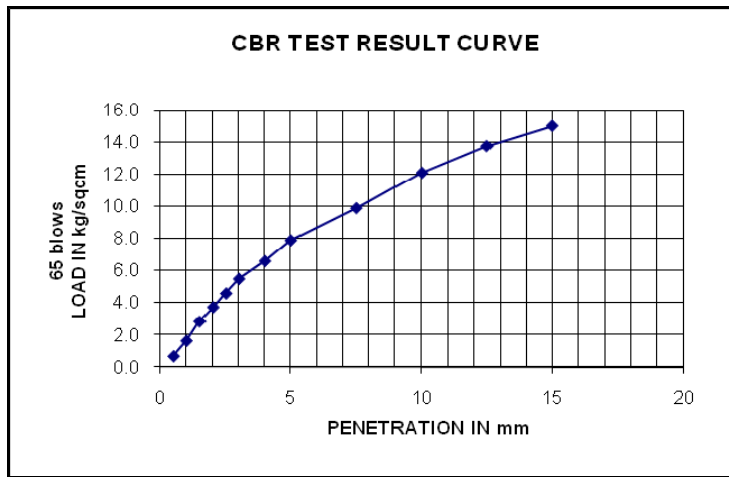
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

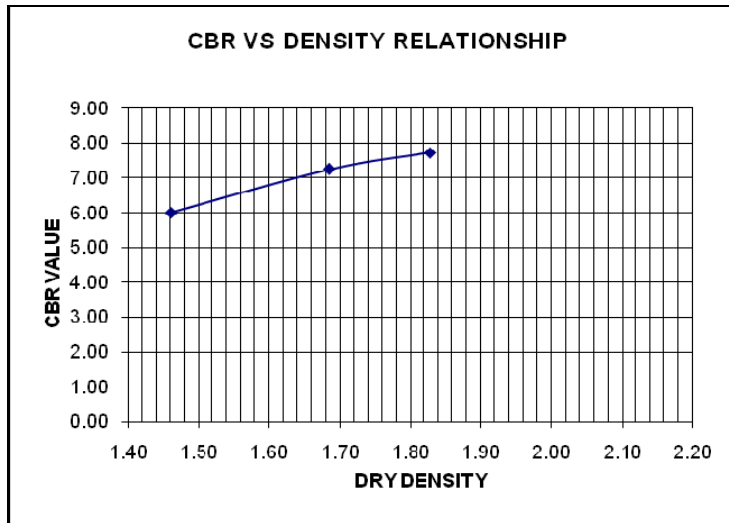
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9262 | 9855 | 10232 | 9680 | 10192 | 10524 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 3922 | 4515 | 4892 | 4340 | 4852 | 5184 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.74 | 2.01 | 2.17 | 1.93 | 2.16 | 2.30 |
| Water Content (%) | 19.3 | 19.1 | 18.9 | 32 | 28 | 26 |
| Dry Density (gms/cc) | 1.46 | 1.68 | 1.83 | 1.46 | 1.68 | 1.83 |

| Penetration (mm) | Penetration Data | | | | | | Proving Ring Used: 1000kg | | | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|--|--|
| | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 | | |
| 0.5 | 11 | 13 | 14 | 0.6 | 0.7 | 0.7 | | | | | | | | | |
| 1.0 | 25 | 30 | 33 | 1.3 | 1.5 | 1.7 | | | | | | | | | |
| 1.5 | 44 | 52 | 57 | 2.2 | 2.6 | 2.9 | | | | | | | | | |
| 2.0 | 58 | 69 | 75 | 2.9 | 3.5 | 3.8 | | | | | | | | | |
| 2.5 | 70 | 84 | 92 | 3.5 | 4.2 | 4.6 | 70 | 3.7 | 4.5 | 4.8 | 5.3 | 6.4 | 6.9 | | |
| 3.0 | 84 | 100 | 110 | 4.2 | 5.0 | 5.5 | | | | | | | | | |
| 4.0 | 104 | 122 | 132 | 5.2 | 6.1 | 6.6 | | | | | | | | | |
| 5.0 | 122 | 146 | 158 | 6.1 | 7.3 | 7.9 | 105 | 6.3 | 7.6 | 8.1 | 6.0 | 7.2 | 7.7 | | |
| 7.5 | 152 | 180 | 198 | 7.6 | 9.0 | 9.9 | | | | | | | | | |
| 10.0 | 186 | 220 | 242 | 9.3 | 11.0 | 12.1 | | | | | | | | | |
| 12.5 | 208 | 250 | 275 | 10.4 | 12.5 | 13.8 | | | | | | | | | |
| 15.0 | 232 | 278 | 300 | 11.6 | 13.9 | 15.0 | | | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 5.29 | 6.43 | 6.86 |
| 5 | 6.00 | 7.24 | 7.71 |



MDD=1.72 gm/cc; 97% of MDD=1.67 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=7.00 (from graph)

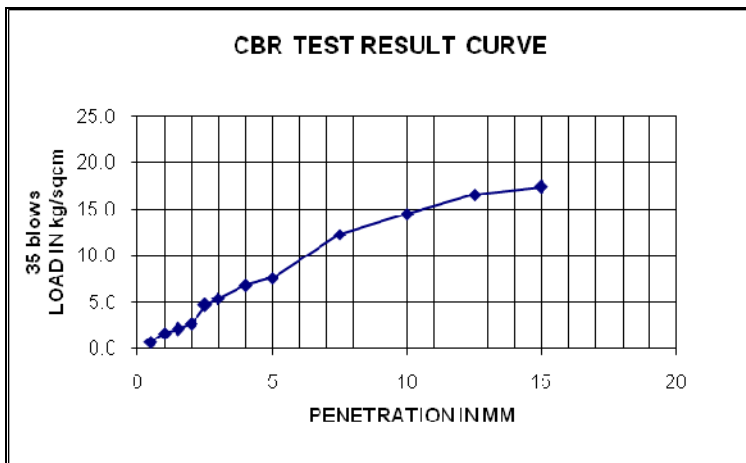
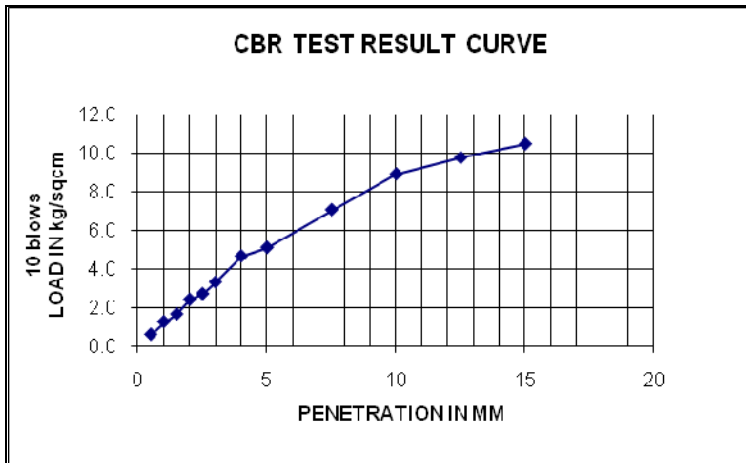
LOCATION: 120+200 km

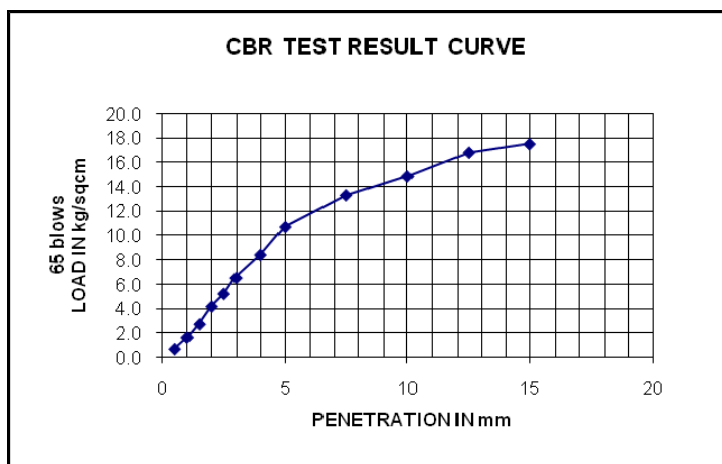
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

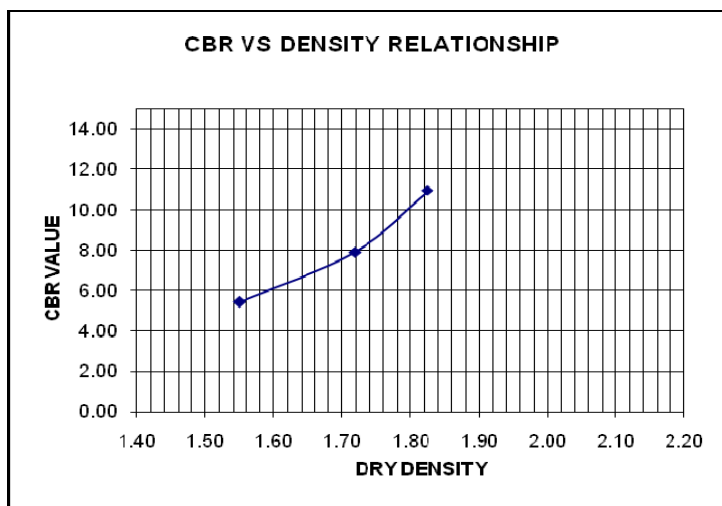
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9500 | 9946 | 10223 | 9943 | 10406 | 10679 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4160 | 4606 | 4883 | 4603 | 5066 | 5339 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.85 | 2.05 | 2.17 | 2.05 | 2.25 | 2.37 |
| Water Content (%) | 19.3 | 19.1 | 18.9 | 32 | 31 | 30 |
| Dry Density (gms/cc) | 1.55 | 1.72 | 1.83 | 1.55 | 1.72 | 1.83 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|------|--------------|-----|------|--|--|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 | | |
| 0.5 | 12 | 13 | 14 | 0.6 | 0.7 | 0.7 | | | | | | | | | |
| 1.0 | 25 | 31 | 33 | 1.3 | 1.6 | 1.7 | | | | | | | | | |
| 1.5 | 33 | 40 | 55 | 1.7 | 2.0 | 2.8 | | | | | | | | | |
| 2.0 | 48 | 52 | 84 | 2.4 | 2.6 | 4.2 | | | | | | | | | |
| 2.5 | 54 | 92 | 105 | 2.7 | 4.6 | 5.3 | 70 | 3.3 | 5.3 | 6.0 | 4.7 | 7.6 | 8.6 | | |
| 3.0 | 66 | 107 | 131 | 3.3 | 5.4 | 6.6 | | | | | | | | | |
| 4.0 | 93 | 135 | 169 | 4.7 | 6.8 | 8.5 | | | | | | | | | |
| 5.0 | 102 | 151 | 215 | 5.1 | 7.6 | 10.8 | 105 | 5.7 | 8.3 | 11.5 | 5.4 | 7.9 | 11.0 | | |
| 7.5 | 141 | 245 | 267 | 7.1 | 12.3 | 13.4 | | | | | | | | | |
| 10.0 | 178 | 289 | 298 | 8.9 | 14.5 | 14.9 | | | | | | | | | |
| 12.5 | 195 | 330 | 337 | 9.8 | 16.5 | 16.9 | | | | | | | | | |
| 15.0 | 209 | 347 | 351 | 10.5 | 17.4 | 17.6 | | | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 4.71 | 7.57 | 8.57 |
| 5 | 5.43 | 7.90 | 11.0 |



MDD=1.65 gm/cc; 97% of MDD=1.60 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=6.10 (from graph)

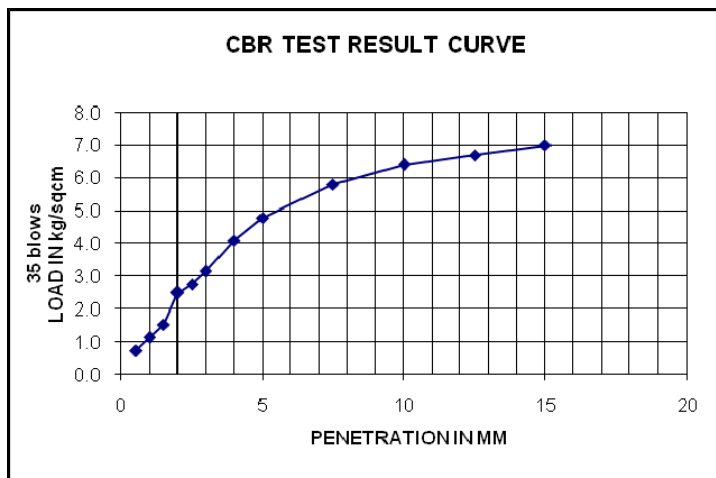
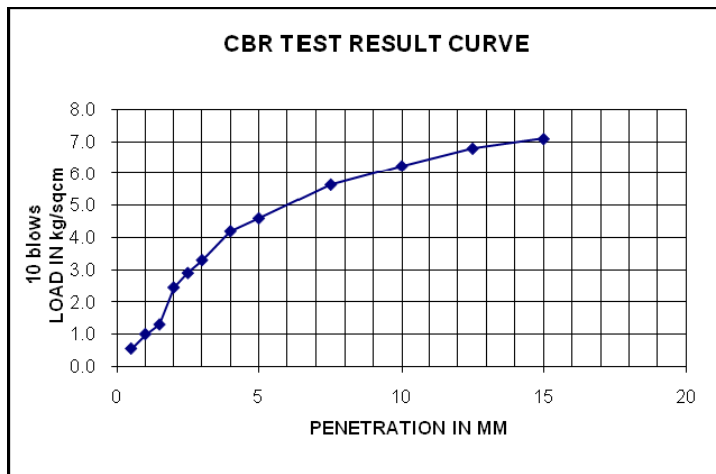
LOCATION: 130+000 km

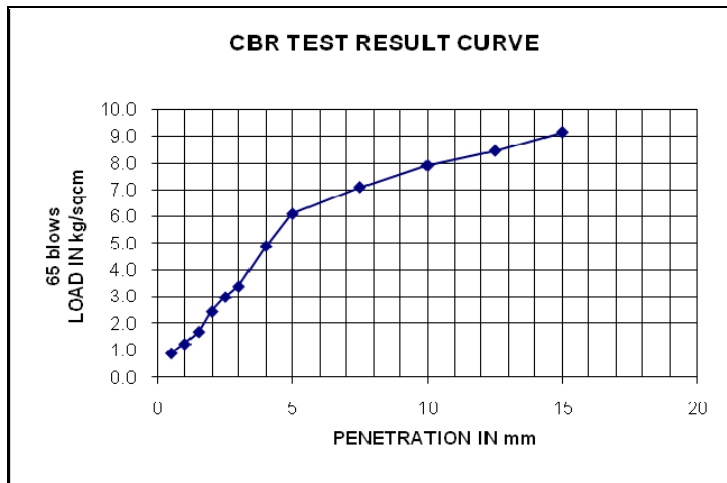
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

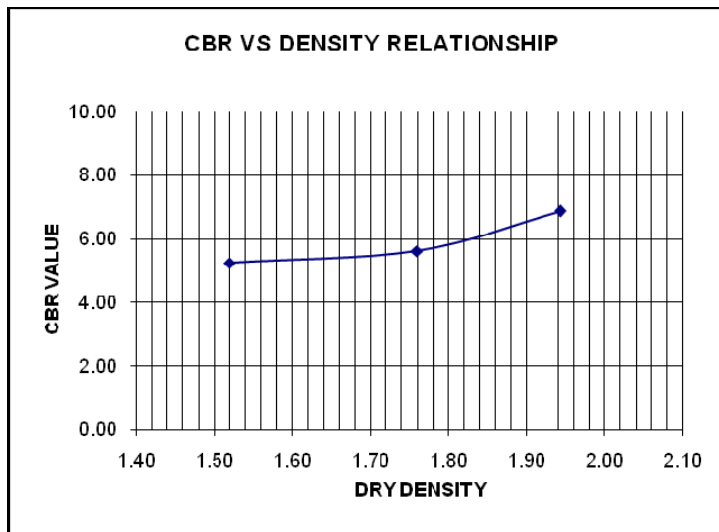
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9366 | 9992 | 10456 | 9954 | 10645 | 11112 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4026 | 4652 | 5116 | 4614 | 5305 | 5772 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.79 | 2.07 | 2.27 | 2.05 | 2.36 | 2.57 |
| Water Content (%) | 17.8 | 17.5 | 17 | 35 | 34 | 32 |
| Dry Density (gms/cc) | 1.52 | 1.76 | 1.94 | 1.52 | 1.76 | 1.94 |

| Penetration n (mm) | Penetration Data | | | | | | Standard Load kg/cm ² | Proving Ring Used: 1000kg | | | | | |
|-----------------------|-------------------------|-------------|-------------|-----------------------|-------------|-------------|--|--------------------------------------|-----|-----|--------------|-----|-----|
| | TEST LOAD | | | | | | | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 11 | 15 | 18 | 0.6 | 0.8 | 0.9 | | | | | | | |
| 1.0 | 20 | 23 | 25 | 1.0 | 1.2 | 1.3 | | | | | | | |
| 1.5 | 26 | 31 | 34 | 1.3 | 1.6 | 1.7 | | | | | | | |
| 2.0 | 49 | 50 | 49 | 2.5 | 2.5 | 2.5 | | | | | | | |
| 2.5 | 58 | 55 | 60 | 2.9 | 2.8 | 3.0 | 70 | 3.8 | 4.0 | 4.1 | 5.4 | 5.7 | 5.9 |
| 3.0 | 66 | 63 | 68 | 3.3 | 3.2 | 3.4 | | | | | | | |
| 4.0 | 84 | 82 | 98 | 4.2 | 4.1 | 4.9 | | | | | | | |
| 5.0 | 92 | 96 | 122 | 4.6 | 4.8 | 6.1 | 105 | 5.5 | 5.9 | 7.2 | 5.2 | 5.6 | 6.9 |
| 7.5 | 113 | 116 | 142 | 5.7 | 5.8 | 7.1 | | | | | | | |
| 10.0 | 125 | 128 | 158 | 6.3 | 6.4 | 7.9 | | | | | | | |
| 12.5 | 136 | 134 | 169 | 6.8 | 6.7 | 8.5 | | | | | | | |
| 15.0 | 142 | 140 | 183 | 7.1 | 7.0 | 9.2 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 5.43 | 5.71 | 5.86 |
| 5 | 5.24 | 5.62 | 6.9 |



MDD=1.70 gm/cc; 97% of MDD=1.65 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=5.50 (from graph)

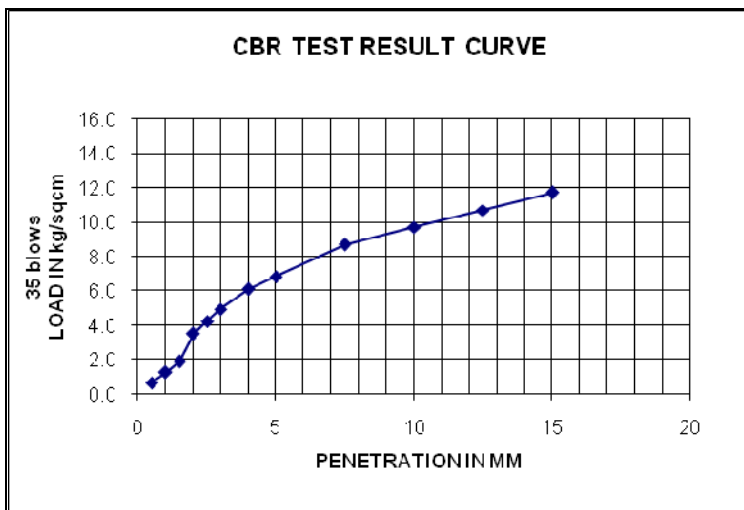
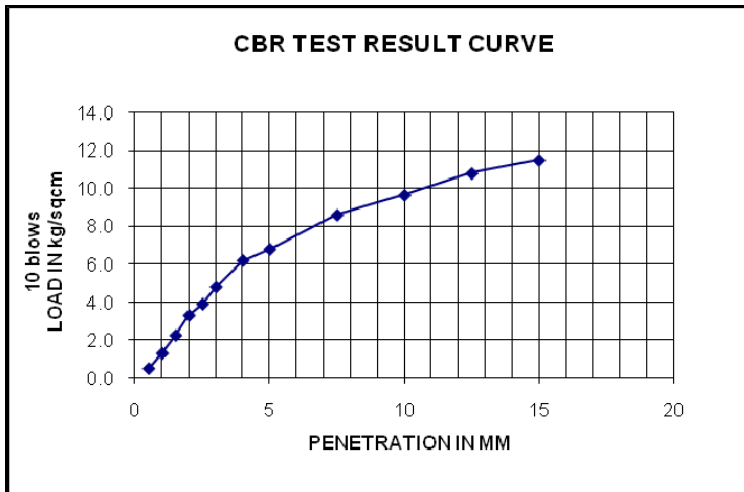
LOCATION: 140+100 km

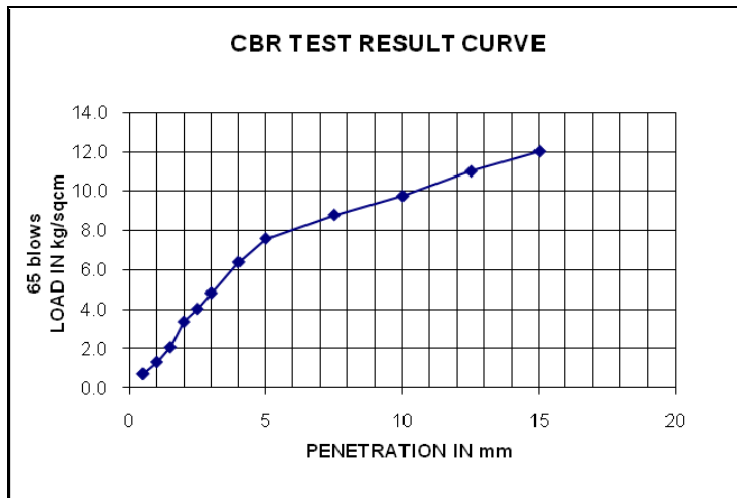
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

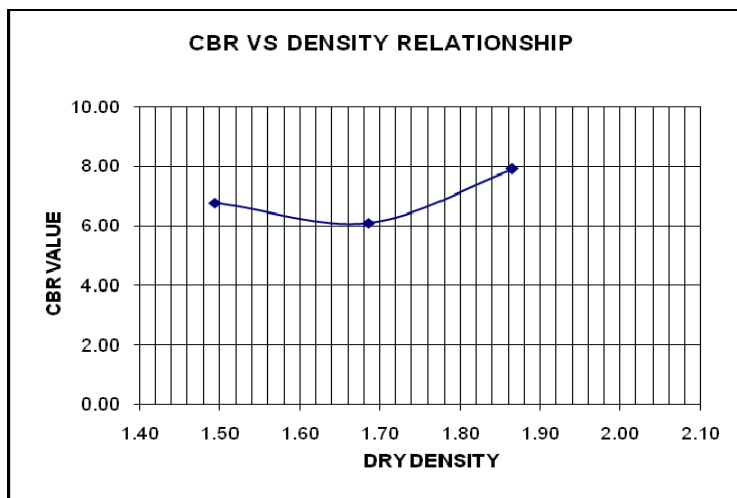
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9255 | 9768 | 10212 | 9712 | 10197 | 10585 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 3915 | 4428 | 4872 | 4372 | 4857 | 5245 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.74 | 1.97 | 2.17 | 1.94 | 2.16 | 2.33 |
| Water Content (%) | 16.4 | 16.7 | 16.1 | 30 | 28 | 25 |
| Dry Density (gms/cc) | 1.49 | 1.69 | 1.87 | 1.49 | 1.69 | 1.87 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 10 | 13 | 15 | 0.5 | 0.7 | 0.8 | | | | | | | |
| 1.0 | 26 | 25 | 27 | 1.3 | 1.3 | 1.4 | | | | | | | |
| 1.5 | 45 | 38 | 42 | 2.3 | 1.9 | 2.1 | | | | | | | |
| 2.0 | 66 | 70 | 68 | 3.3 | 3.5 | 3.4 | | | | | | | |
| 2.5 | 78 | 85 | 81 | 3.9 | 4.3 | 4.1 | 70 | 4.2 | 4.6 | 4.8 | 6.0 | 6.6 | 6.9 |
| 3.0 | 96 | 99 | 97 | 4.8 | 5.0 | 4.9 | | | | | | | |
| 4.0 | 124 | 122 | 128 | 6.2 | 6.1 | 6.4 | | | | | | | |
| 5.0 | 136 | 137 | 152 | 6.8 | 6.9 | 7.6 | 105 | 7.1 | 6.4 | 8.3 | 6.8 | 6.1 | 7.9 |
| 7.5 | 172 | 174 | 176 | 8.6 | 8.7 | 8.8 | | | | | | | |
| 10.0 | 193 | 194 | 195 | 9.7 | 9.7 | 9.8 | | | | | | | |
| 12.5 | 216 | 214 | 220 | 10.8 | 10.7 | 11.0 | | | | | | | |
| 15.0 | 230 | 234 | 240 | 11.5 | 11.7 | 12.0 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 6.00 | 6.57 | 6.86 |
| 5 | 6.76 | 6.10 | 7.90 |



MDD=1.62 gm/cc; 97% of MDD=1.57 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=6.40 (from graph)

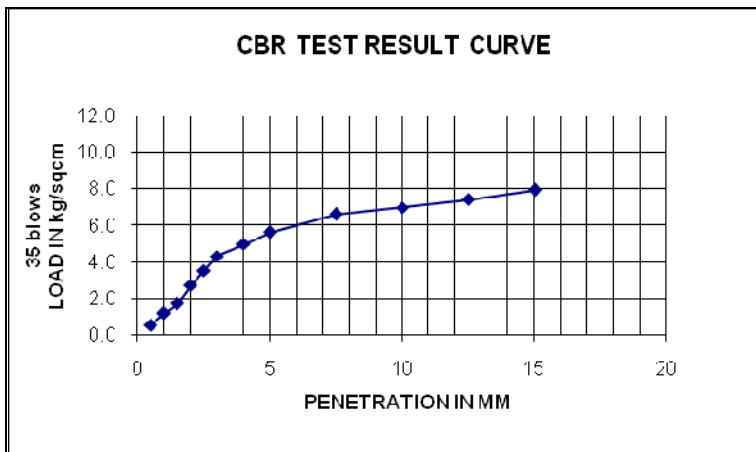
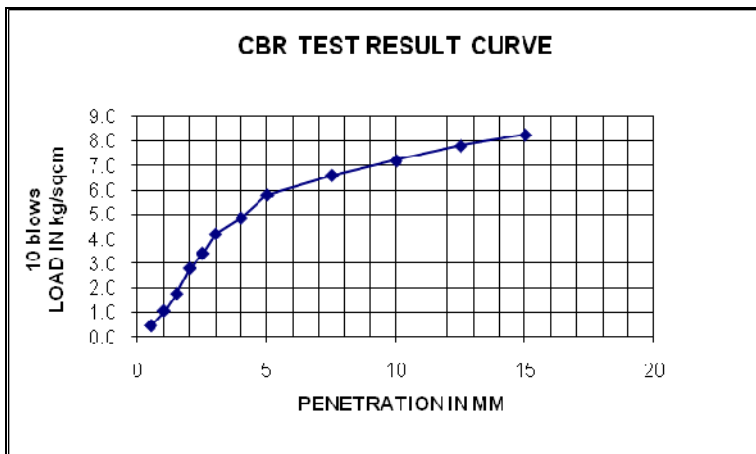
LOCATION: 150+000 km

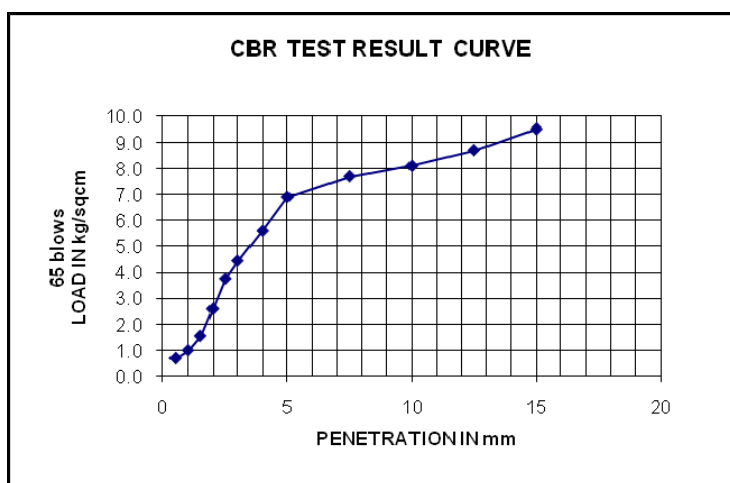
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

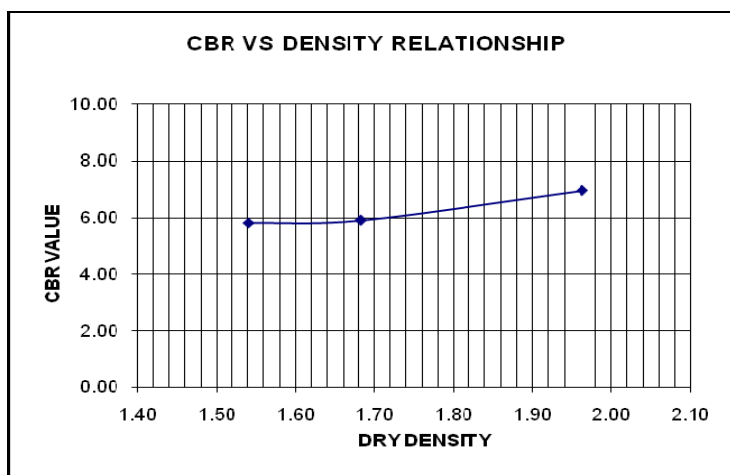
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9256 | 9788 | 10520 | 10087 | 10488 | 11302 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 3916 | 4448 | 5180 | 4747 | 5148 | 5962 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.74 | 1.98 | 2.30 | 2.11 | 2.29 | 2.65 |
| Water Content (%) | 17.8 | 17.5 | 17.3 | 37 | 36 | 35 |
| Dry Density (gms/cc) | 1.54 | 1.68 | 1.96 | 1.54 | 1.68 | 1.96 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 9 | 11 | 14 | 0.5 | 0.6 | 0.7 | | | | | | | |
| 1.0 | 21 | 23 | 20 | 1.1 | 1.2 | 1.0 | | | | | | | |
| 1.5 | 35 | 34 | 31 | 1.8 | 1.7 | 1.6 | | | | | | | |
| 2.0 | 56 | 54 | 52 | 2.8 | 2.7 | 2.6 | | | | | | | |
| 2.5 | 68 | 70 | 75 | 3.4 | 3.5 | 3.8 | 70 | 5.7 | 4.1 | 4.2 | 8.1 | 5.9 | 6.0 |
| 3.0 | 84 | 86 | 89 | 4.2 | 4.3 | 4.5 | | | | | | | |
| 4.0 | 97 | 99 | 112 | 4.9 | 5.0 | 5.6 | | | | | | | |
| 5.0 | 116 | 112 | 138 | 5.8 | 5.6 | 6.9 | 105 | 6.1 | 6.2 | 7.3 | 5.8 | 5.9 | 7.0 |
| 7.5 | 132 | 132 | 154 | 6.6 | 6.6 | 7.7 | | | | | | | |
| 10.0 | 144 | 139 | 162 | 7.2 | 7.0 | 8.1 | | | | | | | |
| 12.5 | 156 | 148 | 174 | 7.8 | 7.4 | 8.7 | | | | | | | |
| 15.0 | 165 | 158 | 190 | 8.3 | 7.9 | 9.5 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 8.14 | 5.86 | 6.00 |
| 5 | 5.81 | 5.90 | 7.0 |



MDD=1.70 gm/cc; 97% of MDD=1.65 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=5.80 (from graph)

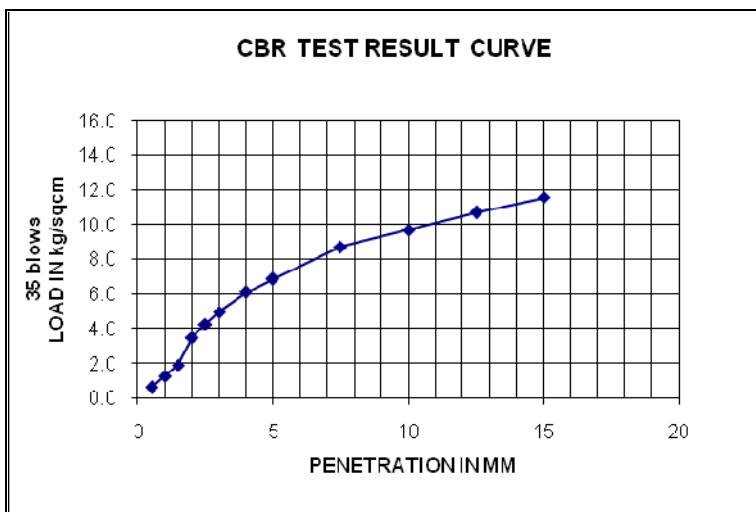
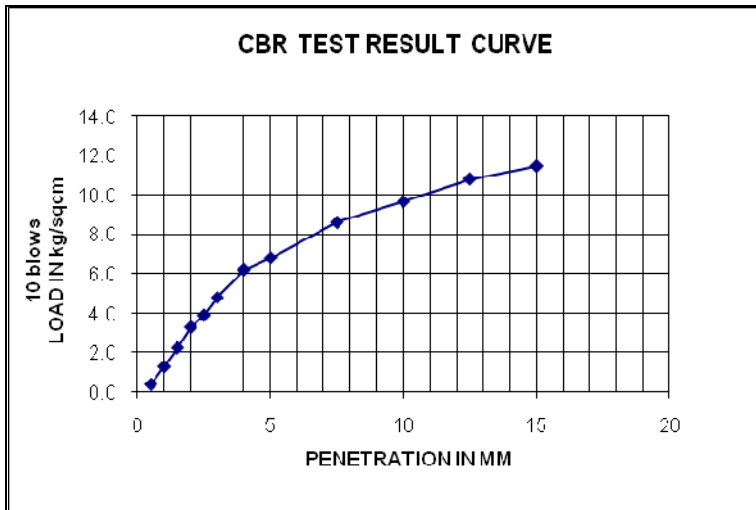
LOCATION: 160+000 km

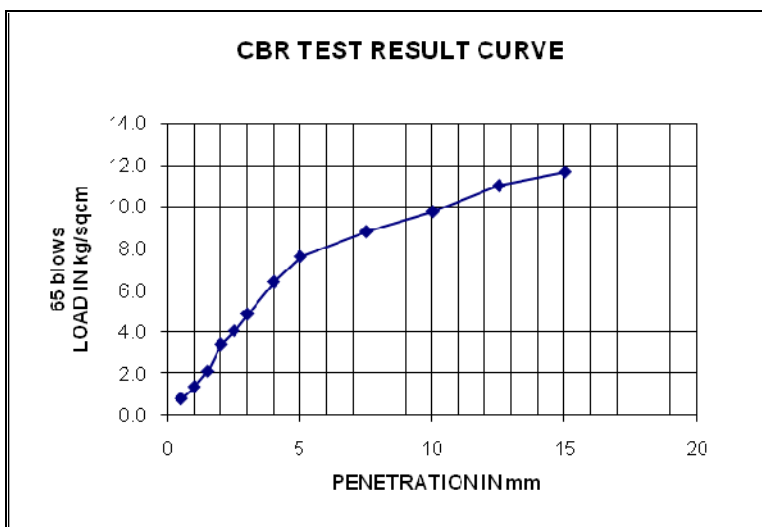
Test condition: Soaked

Nature of Sample: Compacted in 5 layers with 10/35/65 blows of 4.9kg rammer having 45cm drop at OMC

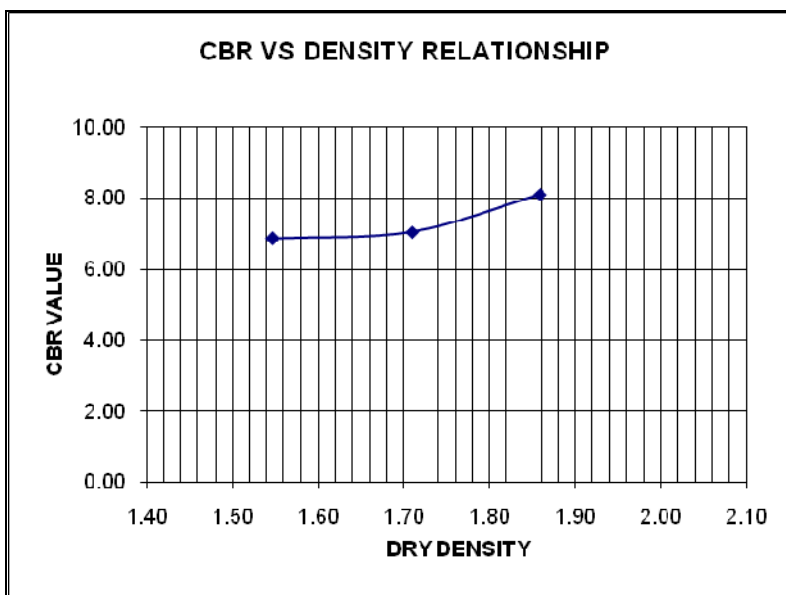
| Water Content and Dry Density Data | Before Soaking | | | After Soaking | | |
|------------------------------------|----------------|----------|----------|---------------|----------|----------|
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows |
| Wt Wet Soil+Mould (gm) | 9432 | 9840 | 10256 | 10037 | 10494 | 10904 |
| Wt Mould (gm) | 5340 | 5340 | 5340 | 5340 | 5340 | 5340 |
| Wt Wet Soil (gm) | 4092 | 4500 | 4916 | 4697 | 5154 | 5564 |
| Vol. Soil (cc) | 2250 | 2250 | 2250 | 2250 | 2250 | 2250 |
| Wet Density (gms/cc) | 1.82 | 2.00 | 2.18 | 2.09 | 2.29 | 2.47 |
| Water Content (%) | 17.6 | 17 | 17.5 | 35 | 34 | 33 |
| Dry Density (gms/cc) | 1.55 | 1.71 | 1.86 | 1.55 | 1.71 | 1.86 |

| Penetration Data | | | | | | | Proving Ring Used: 1000kg | | | | | | |
|------------------|----------------------|----------|----------|-----------------------|----------|----------|----------------------------------|--------------------------------------|-----|-----|--------------|-----|-----|
| Penetration (mm) | TEST LOAD | | | | | | Standard Load kg/cm ² | Corrected Load (kg/cm ²) | | | CBR (%) | | |
| | Proving ring Reading | | | In kg/cm ² | | | | No. of blows | | | No. of blows | | |
| | 10 blows | 35 blows | 65 blows | 10 blows | 35 blows | 65 blows | | 10 | 35 | 65 | 10 | 35 | 65 |
| 0.5 | 8 | 12 | 16 | 0.4 | 0.6 | 0.8 | | | | | | | |
| 1.0 | 26 | 25 | 27 | 1.3 | 1.3 | 1.4 | | | | | | | |
| 1.5 | 45 | 38 | 42 | 2.3 | 1.9 | 2.1 | | | | | | | |
| 2.0 | 66 | 70 | 68 | 3.3 | 3.5 | 3.4 | | | | | | | |
| 2.5 | 78 | 85 | 81 | 3.9 | 4.3 | 4.1 | 70 | 4.3 | 4.8 | 5.0 | 6.1 | 6.9 | 7.1 |
| 3.0 | 96 | 99 | 97 | 4.8 | 5.0 | 4.9 | | | | | | | |
| 4.0 | 124 | 122 | 128 | 6.2 | 6.1 | 6.4 | | | | | | | |
| 5.0 | 136 | 137 | 152 | 6.8 | 6.9 | 7.6 | 105 | 7.2 | 7.4 | 8.5 | 6.9 | 7.0 | 8.1 |
| 7.5 | 172 | 174 | 176 | 8.6 | 8.7 | 8.8 | | | | | | | |
| 10.0 | 193 | 194 | 195 | 9.7 | 9.7 | 9.8 | | | | | | | |
| 12.5 | 216 | 214 | 220 | 10.8 | 10.7 | 11.0 | | | | | | | |
| 15.0 | 229 | 231 | 233 | 11.5 | 11.6 | 11.7 | | | | | | | |





| Penetration (mm) | Soaked CBR (%) | | |
|------------------|----------------|----------|----------|
| | 10 blows | 35 blows | 65 blows |
| 2.5 | 6.14 | 6.86 | 7.14 |
| 5 | 6.86 | 7.05 | 8.10 |



MDD=1.70 gm/cc; 97% of MDD=1.65 gm/cc

The CBR value to be adopted=CBR value of 97% of MDD=6.80 (from graph)

8. SUMMARY OF TEST RESULTS: Sub-grade of existing pavement-

| Sl. No. | Chainage (km) | Sieve Analysis (% Passing by Weight) | | | | | | Atterberg's LL | Limit PL | Plasticity Index | Soil-Classification | Field | | Laboratory | | Soaked CBR at 3 Energy Levels | | | | | | Soaked CBR at 97% of MDD | Unsoaked CBR at 3 Energy Levels | | | | | | Unsoaked CBR at 97% of MDD |
|---------|------------------|---|----------------------|----------------|------------|----------|------------|-------------------|-------------|------------------|---------------------|----------|------------|------------|------------|-------------------------------|------------|----------|------------|----------|------------|-----------------------------|---------------------------------|------------|------|------------|------|------------|-------------------------------|
| | | Data | | Compaction | | 10 Blows | | | | | | 35 Blows | | 65 Blows | | 10 Blows | | 35 Blows | | 65 Blows | | | | | | | | | |
| | | Dry Density (gm/cc) | Water Content (%) | MDD (gm/cc) | OMC (%) | DD | CBR (%) | | | | | DD | CBR (%) | DD | CBR (%) | DD | CBR (%) | DD | CBR (%) | DD | CBR (%) | | DD | CBR (%) | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | DD | CBR (%) | DD | CBR (%) | |
| 1 | 40+100 | 100 | 100 | 99.76 | 93.17 | 80.96 | 73.43 | 34.53 | 27.39 | 7.14 | CL | 0.19 | 19.00 | 1.76 | 17.1 | 1.50 | 5.70 | 1.72 | 6.30 | 1.86 | 6.90 | 6.3 | 1.50 | 5.82 | 1.72 | 6.85 | 1.86 | 7.40 | 7.1 |
| 2 | 42+000 | 100 | 100 | 98.40 | 91.7 | 76.78 | 64.29 | 32.54 | 23.09 | 9.45 | CL | 0.15 | 15.00 | 1.79 | 17.4 | 1.71 | 5.71 | 1.90 | 5.90 | 2.09 | 6.63 | 6.4 | 1.71 | 5.84 | 1.90 | 6.41 | 2.09 | 7.11 | 6.9 |
| 3 | 43+100 | 100 | 100 | 99.11 | 92.37 | 74.35 | 62.58 | 34.34 | 26.76 | 7.58 | CL | 0.14 | 13.50 | 1.85 | 18.0 | 1.64 | 5.98 | 1.83 | 6.16 | 2.01 | 6.93 | 6.0 | 1.64 | 6.11 | 1.83 | 6.70 | 2.01 | 7.43 | 7.2 |
| 4 | 44+000 | 100 | 100 | 98.53 | 91.83 | 77.47 | 65.26 | 31.54 | 23.30 | 8.24 | CL | 0.13 | 13.00 | 1.86 | 18.1 | 1.78 | 5.27 | 1.96 | 5.45 | 2.15 | 6.13 | 6.4 | 1.78 | 5.38 | 1.96 | 5.93 | 2.15 | 6.58 | 6.4 |
| 5 | 45+000 | 100 | 100 | 99.33 | 92.57 | 71.73 | 61.26 | 29.34 | 19.80 | 9.54 | CL | 0.14 | 14.00 | 1.84 | 17.9 | 1.81 | 4.95 | 1.99 | 5.14 | 2.18 | 5.77 | 6.2 | 1.81 | 5.06 | 1.99 | 5.58 | 2.18 | 6.19 | 6.1 |
| 6 | 46+150 | 100 | 100 | 98.13 | 91.45 | 80.94 | 68.23 | 28.54 | 20.70 | 7.84 | CL | 0.12 | 11.50 | 1.80 | 17.5 | 1.65 | 5.63 | 1.84 | 5.81 | 2.02 | 6.53 | 6.1 | 1.65 | 5.75 | 1.84 | 6.32 | 2.02 | 7.01 | 6.8 |
| 7 | 47+000 | 100 | 100 | 98.85 | 92.46 | 71.23 | 31.05 | 35.83 | 25.65 | 10.18 | CL | 0.11 | 10.50 | 1.90 | 18.5 | 1.74 | 6.37 | 1.92 | 6.55 | 2.11 | 7.37 | 6.4 | 1.74 | 6.51 | 1.92 | 7.12 | 2.11 | 7.90 | 7.6 |
| 8 | 48+000 | 100 | 100 | 98.23 | 93.24 | 71.07 | 57.87 | 30.43 | 21.00 | 9.43 | CL | 0.17 | 16.50 | 1.89 | 18.4 | 1.83 | 6.21 | 2.02 | 6.40 | 2.20 | 7.19 | 6.3 | 1.83 | 6.34 | 2.02 | 6.95 | 2.20 | 7.71 | 7.5 |
| 9 | 49+000 | 100 | 100 | 99.63 | 93.59 | 79.54 | 74.53 | 29.01 | 22.58 | 6.43 | CL | 0.17 | 17.00 | 1.85 | 18.0 | 1.75 | 6.31 | 1.93 | 6.49 | 2.12 | 7.29 | 6.4 | 1.75 | 6.44 | 1.93 | 7.06 | 2.12 | 7.83 | 7.6 |
| 10 | 50+150 | 100 | 100 | 98.02 | 91.3 | 73.78 | 63.08 | 27.54 | 20.00 | 7.54 | CL | 0.20 | 20.00 | 1.70 | 16.6 | 1.56 | 6.30 | 1.77 | 7.10 | 1.86 | 7.00 | 7.0 | 1.56 | 6.44 | 1.77 | 7.72 | 1.86 | 7.51 | 7.7 |
| 11 | 51+000 | 100 | 100 | 98.44 | 91.69 | 72.94 | 62.35 | 31.34 | 22.91 | 8.43 | CL | 0.11 | 10.50 | 1.86 | 18.1 | 1.70 | 6.45 | 1.89 | 6.64 | 2.08 | 7.46 | 6.5 | 1.70 | 6.59 | 1.89 | 7.22 | 2.08 | 8.00 | 7.7 |
| 12 | 52+000 | 100 | 100 | 99.00 | 92.21 | 69.74 | 60.16 | 30.67 | 21.37 | 9.30 | CL | 0.11 | 11.00 | 1.88 | 18.3 | 1.72 | 5.15 | 1.91 | 5.34 | 2.09 | 6.00 | 6.4 | 1.72 | 5.26 | 1.91 | 5.80 | 2.09 | 6.44 | 6.3 |
| 13 | 53+100 | 100 | 100 | 99.33 | 92.52 | 87.44 | 74.96 | 31.53 | 24.39 | 7.14 | CL | 0.09 | 8.50 | 1.91 | 18.6 | 1.75 | 4.92 | 1.94 | 5.11 | 2.12 | 5.74 | 6.2 | 1.75 | 5.03 | 1.94 | 5.55 | 2.12 | 6.16 | 6.0 |
| 14 | 54+000 | 100 | 100 | 97.44 | 90.76 | 85.04 | 72.87 | 28.78 | 22.25 | 6.53 | CL | 0.10 | 10.00 | 1.78 | 17.3 | 1.63 | 6.01 | 1.81 | 6.20 | 2.00 | 6.96 | 6.0 | 1.63 | 6.14 | 1.81 | 6.73 | 2.00 | 7.47 | 7.2 |
| 15 | 55+000 | 100 | 100 | 96.23 | 90.23 | 88.51 | 73.19 | 27.56 | 21.34 | 6.22 | CL | 0.08 | 7.50 | 1.77 | 17.2 | 1.62 | 6.57 | 1.80 | 6.76 | 1.99 | 7.59 | 6.6 | 1.62 | 6.71 | 1.80 | 7.34 | 1.99 | 8.15 | 7.9 |
| 16 | 56+000 | 100 | 100 | 97.00 | 90.97 | 83.44 | 73.7 | 29.43 | 22.09 | 7.34 | CL | 0.12 | 11.50 | 1.84 | 17.9 | 1.68 | 6.36 | 1.87 | 6.54 | 2.06 | 7.35 | 6.4 | 1.68 | 6.50 | 1.87 | 7.11 | 2.06 | 7.89 | 7.6 |
| 17 | 57+150 | 100 | 100 | 98.53 | 92.4 | 78.07 | 69.26 | 31.76 | 21.31 | 10.45 | CL | 0.13 | 12.50 | 1.79 | 17.4 | 1.64 | 5.73 | 1.82 | 5.92 | 2.01 | 6.65 | 6.4 | 1.64 | 5.86 | 1.82 | 6.43 | 2.01 | 7.14 | 6.9 |
| 18 | 58+000 | 100 | 100 | 97.44 | 91.38 | 75.94 | 66.98 | 29.76 | 19.0 | 7.6 | CL | 0.12 | 11.50 | 1.84 | 17.9 | 1.68 | 6.36 | 1.87 | 6.54 | 2.06 | 7.35 | 6.4 | 1.68 | 6.50 | 1.87 | 7.11 | 2.06 | 7.89 | 7.6 |
| 19 | 59+000 | 100 | 100 | 98.53 | 92.4 | 81.73 | 72.17 | 30.53 | 21.99 | 8.54 | CL | 0.15 | 15.00 | 1.86 | 18.1 | 1.70 | 6.01 | 1.89 | 6.20 | 2.08 | 6.96 | 6.1 | 1.70 | 6.14 | 1.89 | 6.73 | 2.08 | 7.47 | 7.2 |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|--------|-----|-----|-------|-------|-------|-------|-------|-------|-------|----|------|-------|------|------|------|------|------|------|------|------|-----|------|------|------|------|------|------|-----|
| 20 | 60+000 | 100 | 100 | 97.47 | 91.4 | 86.07 | 76.06 | 29.14 | 21.60 | 7.54 | CL | 0.19 | 19.00 | 1.69 | 16.2 | 1.46 | 4.57 | 1.69 | 6.43 | 1.82 | 6.57 | 6.0 | 1.46 | 4.67 | 1.69 | 6.99 | 1.82 | 7.05 | 6.7 |
| 21 | 61+000 | 100 | 100 | 97.32 | 89.29 | 89.41 | 74.6 | 29.11 | 21.13 | 7.98 | CL | 0.19 | 19.00 | 1.85 | 18.0 | 1.76 | 4.96 | 1.94 | 5.15 | 2.13 | 5.78 | 5.5 | 1.76 | 5.07 | 1.94 | 5.59 | 2.13 | 6.21 | 6.1 |
| 22 | 62+000 | 100 | 100 | 98.23 | 89.51 | 78.07 | 67.95 | 28.34 | 21.47 | 6.87 | CL | 0.13 | 12.50 | 1.84 | 17.9 | 1.75 | 5.67 | 1.93 | 5.86 | 2.12 | 6.58 | 5.6 | 1.75 | 5.79 | 1.93 | 6.37 | 2.12 | 7.06 | 6.9 |
| 23 | 63+000 | 100 | 100 | 98.13 | 89.42 | 77.99 | 70.16 | 27.54 | 20.00 | 7.54 | CL | 0.16 | 16.00 | 1.88 | 18.3 | 1.79 | 5.59 | 1.97 | 5.77 | 2.16 | 6.49 | 6.4 | 1.79 | 5.71 | 1.97 | 6.27 | 2.16 | 6.96 | 6.8 |
| 24 | 64+100 | 100 | 100 | 99.24 | 90.43 | 78.86 | 68.65 | 32.54 | 23.01 | 9.53 | CL | 0.12 | 12.00 | 1.90 | 18.5 | 1.81 | 6.00 | 1.99 | 6.18 | 2.18 | 6.95 | 6.1 | 1.81 | 6.13 | 1.99 | 6.72 | 2.18 | 7.46 | 7.2 |
| 25 | 65+000 | 100 | 100 | 97.44 | 88.8 | 80.74 | 70.31 | 31.34 | 21.39 | 9.95 | CL | 0.15 | 15.00 | 1.91 | 18.6 | 1.82 | 6.39 | 2.00 | 6.58 | 2.19 | 7.39 | 6.4 | 1.82 | 6.53 | 2.00 | 7.15 | 2.19 | 7.93 | 7.7 |
| 26 | 66+000 | 100 | 100 | 96.23 | 87.69 | 76.5 | 66.57 | 29.53 | 20.30 | 9.23 | CL | 0.12 | 12.00 | 1.85 | 18.0 | 1.76 | 5.06 | 1.94 | 5.24 | 2.13 | 5.89 | 6.1 | 1.76 | 5.17 | 1.94 | 5.70 | 2.13 | 6.32 | 6.2 |
| 27 | 67+000 | 100 | 100 | 98.09 | 89.39 | 74.67 | 64.94 | 29.95 | 21.21 | 8.74 | CL | 0.10 | 10.00 | 1.84 | 17.9 | 1.75 | 5.57 | 1.93 | 5.75 | 2.12 | 6.46 | 5.6 | 1.75 | 5.68 | 1.93 | 6.25 | 2.12 | 6.93 | 6.7 |
| 28 | 68+000 | 100 | 100 | 98.25 | 89.53 | 78.08 | 67.4 | 22.05 | 21.69 | 6.0 | CL | 0.16 | 16.00 | 1.86 | 18.3 | 1.79 | 5.59 | 1.97 | 5.77 | 2.16 | 6.49 | 6.4 | 1.79 | 5.71 | 1.97 | 6.27 | 2.16 | 6.96 | 6.8 |
| 29 | 69+000 | 100 | 100 | 99.20 | 87.79 | 90.42 | 72.4 | 27.85 | 22.75 | 5.10 | CL | 0.08 | 8.00 | 1.78 | 17.3 | 1.69 | 5.17 | 1.87 | 5.36 | 2.06 | 6.02 | 6.5 | 1.69 | 5.28 | 1.87 | 5.82 | 2.06 | 6.46 | 6.3 |
| 30 | 70+120 | 100 | 100 | 98.53 | 89.83 | 75.07 | 67.64 | 28.74 | 22.20 | 6.54 | CL | 0.15 | 15.00 | 1.70 | 16.6 | 1.55 | 5.70 | 1.74 | 5.90 | 1.87 | 6.00 | 5.9 | 1.55 | 5.82 | 1.74 | 6.41 | 1.87 | 6.44 | 6.7 |
| 31 | 71+000 | 100 | 100 | 97.66 | 89.04 | 77.44 | 69.8 | 29.53 | 21.99 | 7.54 | CL | 0.12 | 11.50 | 1.79 | 17.4 | 1.66 | 5.27 | 1.85 | 5.45 | 2.03 | 6.13 | 6.5 | 1.66 | 5.38 | 1.85 | 5.93 | 2.03 | 6.58 | 6.4 |
| 32 | 72+000 | 100 | 100 | 98.05 | 89.39 | 74.71 | 67.31 | 30.43 | 22.29 | 8.14 | CL | 0.16 | 15.50 | 1.80 | 17.5 | 1.67 | 5.57 | 1.86 | 5.75 | 2.04 | 6.46 | 6.0 | 1.67 | 5.68 | 1.86 | 6.25 | 2.04 | 6.93 | 6.7 |
| 33 | 73+150 | 100 | 100 | 99.00 | 90.26 | 80.91 | 72.98 | 32.54 | 23.01 | 9.53 | CL | 0.17 | 16.50 | 1.78 | 17.3 | 1.65 | 5.44 | 1.84 | 5.62 | 2.02 | 6.32 | 5.6 | 1.65 | 5.56 | 1.84 | 6.11 | 2.02 | 6.78 | 6.6 |
| 34 | 74+000 | 100 | 100 | 97.44 | 88.84 | 74.25 | 66.89 | 31.34 | 25.22 | 6.12 | CL | 0.15 | 14.50 | 1.88 | 18.3 | 1.75 | 5.79 | 1.94 | 5.97 | 2.12 | 6.71 | 5.8 | 1.75 | 5.91 | 1.94 | 6.49 | 2.12 | 7.20 | 7.0 |
| 35 | 75+000 | 100 | 100 | 98.24 | 89.57 | 87.44 | 78.96 | 29.76 | 23.22 | 6.54 | CL | 0.13 | 13.00 | 1.89 | 18.4 | 1.76 | 5.15 | 1.95 | 5.34 | 2.13 | 6.00 | 6.4 | 1.76 | 5.26 | 1.95 | 5.80 | 2.13 | 6.44 | 6.3 |
| 36 | 76+000 | 100 | 100 | 99.03 | 85.54 | 66.76 | 29.63 | 25.36 | 19.36 | 6.00 | CL | 0.10 | 10.00 | 1.77 | 17.2 | 1.64 | 6.60 | 1.83 | 6.79 | 2.01 | 7.63 | 6.7 | 1.64 | 6.74 | 1.83 | 7.38 | 2.01 | 8.18 | 7.9 |
| 37 | 77+000 | 100 | 100 | 97.86 | 88.15 | 73.45 | 44.59 | 27.87 | 17.33 | 10.54 | CL | 0.09 | 8.50 | 1.76 | 17.1 | 1.63 | 6.39 | 1.82 | 6.58 | 2.00 | 7.39 | 6.4 | 1.63 | 6.53 | 1.82 | 7.15 | 2.00 | 7.93 | 7.7 |
| 38 | 78+000 | 100 | 100 | 97.22 | 87.57 | 80.74 | 61.26 | 26.57 | 16.74 | 9.83 | CL | 0.08 | 8.00 | 1.78 | 17.3 | 1.65 | 5.59 | 1.84 | 5.77 | 2.02 | 6.49 | 6.0 | 1.65 | 5.71 | 1.84 | 6.27 | 2.02 | 6.96 | 6.8 |
| 39 | 79+000 | 100 | 100 | 97.48 | 87.8 | 74.73 | 56.77 | 28.73 | 21.19 | 7.54 | CL | 0.07 | 7.00 | 1.93 | 18.7 | 1.79 | 5.98 | 1.98 | 6.16 | 2.16 | 6.93 | 6.0 | 1.79 | 6.11 | 1.98 | 6.70 | 2.16 | 7.43 | 7.2 |
| 40 | 80+000 | 100 | 100 | 97.38 | 91.6 | 65.81 | 29.07 | 27.34 | 21.55 | 5.79 | CL | 0.14 | 14.00 | 1.68 | 17.2 | 1.50 | 6.30 | 1.73 | 7.10 | 1.82 | 7.00 | 7.0 | 1.50 | 6.44 | 1.73 | 7.72 | 1.82 | 7.51 | 7.7 |
| 41 | 81+000 | 100 | 100 | 98.63 | 87.85 | 68.94 | 55.45 | 29.54 | 23.01 | 6.53 | CL | 0.10 | 9.50 | 1.84 | 17.9 | 1.69 | 6.54 | 1.88 | 6.72 | 2.06 | 7.56 | 6.6 | 1.69 | 6.68 | 1.88 | 7.31 | 2.06 | 8.11 | 7.8 |
| 42 | 82+000 | 100 | 100 | 98.53 | 87.76 | 74.74 | 67.93 | 30.43 | 24.56 | 5.87 | CL | 0.08 | 7.50 | 1.86 | 18.1 | 1.71 | 6.44 | 1.90 | 6.63 | 2.08 | 7.45 | 6.5 | 1.71 | 6.58 | 1.90 | 7.20 | 2.08 | 7.99 | 7.7 |
| 43 | 83+100 | 100 | 100 | 97.75 | 87.07 | 77.67 | 70.63 | 31.57 | 25.03 | 6.54 | CL | 0.11 | 11.00 | 1.85 | 18.0 | 1.70 | 5.13 | 1.89 | 5.32 | 2.07 | 5.97 | 6.5 | 1.70 | 5.24 | 1.89 | 5.78 | 2.07 | 6.41 | 6.3 |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|---------|-----|-----|-------|-------|-------|-------|-------|-------|-------|----|------|-------|------|------|------|------|------|------|------|------|-----|------|------|------|------|------|------|-----|
| 44 | 84+000 | 100 | 100 | 99.03 | 88.21 | 81.34 | 74.02 | 32.53 | 24.00 | 8.53 | CL | 0.13 | 12.50 | 1.83 | 17.8 | 1.68 | 5.54 | 1.87 | 5.73 | 2.05 | 6.44 | 6.1 | 1.68 | 5.66 | 1.87 | 6.23 | 2.05 | 6.91 | 6.7 |
| 45 | 85+000 | 100 | 100 | 89.63 | 79.85 | 74.74 | 67.93 | 29.13 | 19.98 | 9.15 | CL | 0.17 | 17.00 | 1.78 | 17.3 | 1.63 | 6.15 | 1.82 | 6.33 | 2.01 | 7.12 | 6.2 | 1.63 | 6.28 | 1.82 | 6.88 | 2.01 | 7.64 | 7.4 |
| 46 | 86+000 | 100 | 100 | 99.59 | 88.71 | 85.31 | 72.2 | 28.52 | 21.54 | 6.98 | CL | 0.09 | 8.50 | 1.77 | 17.2 | 1.62 | 5.03 | 1.81 | 5.21 | 2.00 | 5.86 | 6.4 | 1.62 | 5.13 | 1.81 | 5.66 | 2.00 | 6.28 | 6.2 |
| 47 | 87+150 | 100 | 100 | 97.13 | 86.52 | 70.74 | 57.6 | 27.43 | 19.92 | 7.51 | CL | 0.11 | 11.00 | 1.75 | 17.0 | 1.61 | 6.53 | 1.79 | 6.71 | 1.98 | 7.54 | 6.6 | 1.61 | 6.67 | 1.79 | 7.30 | 1.98 | 8.09 | 7.8 |
| 48 | 88+000 | 100 | 100 | 97.24 | 86.62 | 66.94 | 53.56 | 28.54 | 22.90 | 5.64 | CL | 0.19 | 19.00 | 1.85 | 18.0 | 1.70 | 5.97 | 1.89 | 6.15 | 2.07 | 6.91 | 6.0 | 1.70 | 6.10 | 1.89 | 6.69 | 2.07 | 7.42 | 7.2 |
| 49 | 89+000 | 100 | 100 | 96.59 | 78.58 | 84.65 | 74.73 | 27.65 | 22.34 | 5.31 | CL | 0.12 | 12.00 | 1.86 | 18.1 | 1.71 | 6.21 | 1.90 | 6.40 | 2.08 | 7.19 | 6.3 | 1.71 | 6.34 | 1.90 | 6.95 | 2.08 | 7.71 | 7.5 |
| 50 | 90+000 | 100 | 100 | 98.31 | 97.03 | 89.63 | 75.29 | 26.15 | 19.82 | 6.33 | CL | 0.11 | 11.00 | 1.68 | 16.5 | 1.50 | 5.14 | 1.72 | 7.14 | 1.88 | 8.29 | 7.0 | 1.50 | 5.25 | 1.72 | 7.76 | 1.88 | 8.90 | 7.8 |
| 51 | 91+000 | 100 | 100 | 97.73 | 93.68 | 80.94 | 61.26 | 27.56 | 21.46 | 6.10 | CL | 0.13 | 13.00 | 1.75 | 17.0 | 1.66 | 5.65 | 1.84 | 5.84 | 2.03 | 6.56 | 6.4 | 1.66 | 5.77 | 1.84 | 6.34 | 2.03 | 7.04 | 6.8 |
| 52 | 92+000 | 100 | 100 | 99.60 | 94.44 | 90.41 | 74.07 | 27.36 | 20.13 | 7.23 | CL | 0.12 | 11.50 | 1.78 | 17.3 | 1.69 | 5.69 | 1.87 | 5.88 | 2.06 | 6.60 | 5.8 | 1.69 | 5.81 | 1.87 | 6.39 | 2.06 | 7.09 | 6.9 |
| 53 | 93+000 | 100 | 100 | 98.23 | 90.35 | 83.63 | 71.49 | 29.53 | 23.41 | 6.12 | CL | 0.13 | 13.00 | 1.88 | 18.3 | 1.79 | 6.08 | 1.97 | 6.27 | 2.16 | 7.04 | 6.1 | 1.79 | 6.21 | 1.97 | 6.81 | 2.16 | 7.56 | 7.3 |
| 54 | 94+000 | 100 | 100 | 98.63 | 95.55 | 88.55 | 72.13 | 28.76 | 21.36 | 7.40 | CL | 0.16 | 15.50 | 1.87 | 18.2 | 1.78 | 5.01 | 1.96 | 5.20 | 2.15 | 5.84 | 6.0 | 1.78 | 5.12 | 1.96 | 5.65 | 2.15 | 6.27 | 6.1 |
| 55 | 95+100 | 100 | 100 | 97.72 | 91.55 | 83.44 | 74.03 | 29.41 | 23.88 | 5.53 | CL | 0.10 | 9.50 | 1.84 | 17.9 | 1.75 | 4.95 | 1.93 | 5.14 | 2.12 | 5.77 | 5.9 | 1.75 | 5.06 | 1.93 | 5.58 | 2.12 | 6.19 | 6.1 |
| 56 | 96+000 | 100 | 100 | 97.51 | 92.33 | 85.24 | 75.65 | 28.76 | 21.64 | 7.12 | CL | 0.08 | 8.00 | 1.82 | 17.7 | 1.73 | 6.16 | 1.91 | 6.34 | 2.10 | 7.13 | 6.2 | 1.73 | 6.29 | 1.91 | 6.89 | 2.10 | 7.65 | 7.4 |
| 57 | 97+050 | 100 | 100 | 97.13 | 91.97 | 80.77 | 71.62 | 28.34 | 19.80 | 8.54 | CL | 0.12 | 11.50 | 1.76 | 17.1 | 1.67 | 6.39 | 1.85 | 6.58 | 2.04 | 7.39 | 6.4 | 1.67 | 6.53 | 1.85 | 7.15 | 2.04 | 7.93 | 7.7 |
| 58 | 98+100 | 100 | 100 | 97.83 | 92.63 | 77.47 | 68.65 | 27.84 | 22.00 | 6.54 | CL | 0.11 | 11.50 | 1.84 | 18.1 | 1.75 | 5.84 | 1.87 | 6.34 | 2.06 | 7.04 | | | | | | | | 6.8 |
| 59 | 99+000 | 100 | 100 | 97.77 | 92.57 | 72.09 | 63.81 | 29.43 | 23.19 | 6.24 | CL | 0.11 | 10.50 | 1.86 | 18.1 | 1.77 | 5.68 | 1.95 | 5.87 | 2.14 | 6.59 | 5.7 | 1.77 | 5.80 | 1.95 | 6.38 | 2.14 | 7.07 | 6.9 |
| 60 | 100+100 | 100 | 100 | 98.53 | 96.7 | 74.96 | 66.39 | 30.53 | 22.99 | 7.54 | CL | 0.15 | 15.00 | 1.69 | 16.6 | 1.54 | 6.30 | 1.77 | 7.90 | 1.84 | 7.00 | 7.0 | 1.54 | 6.44 | 1.77 | 8.59 | 1.84 | 7.51 | 8.0 |
| 61 | 101+000 | 100 | 100 | 98.64 | 93.39 | 69.67 | 61.63 | 29.76 | 23.31 | 6.45 | CL | 0.18 | 17.50 | 1.84 | 17.9 | 1.80 | 5.27 | 1.98 | 5.45 | 2.17 | 6.13 | 5.6 | 1.80 | 5.38 | 1.98 | 5.93 | 2.17 | 6.58 | 6.4 |
| 62 | 102+000 | 100 | 100 | 98.20 | 92.98 | 70.96 | 62.79 | 28.34 | 18.60 | 9.74 | CL | 0.16 | 16.00 | 1.74 | 16.9 | 1.70 | 5.97 | 1.88 | 6.15 | 2.07 | 6.91 | 6.0 | 1.70 | 6.10 | 1.88 | 6.69 | 2.07 | 7.42 | 7.2 |
| 63 | 103+150 | 100 | 100 | 99.00 | 93.73 | 81.44 | 72.23 | 27.21 | 18.67 | 8.54 | CL | 0.15 | 14.50 | 1.78 | 17.3 | 1.74 | 5.06 | 1.92 | 5.24 | 2.11 | 5.89 | 5.5 | 1.74 | 5.17 | 1.92 | 5.70 | 2.11 | 6.32 | 6.2 |
| 64 | 104+000 | 100 | 100 | 99.13 | 94.77 | 82.74 | 73.4 | 27.43 | 19.89 | 7.54 | CL | 0.20 | 19.50 | 1.86 | 18.1 | 1.82 | 5.19 | 2.01 | 5.38 | 2.19 | 6.05 | 5.9 | 1.82 | 5.31 | 2.01 | 5.85 | 2.19 | 6.49 | 6.3 |
| 65 | 105+000 | 100 | 100 | 99.24 | 93.96 | 84.99 | 75.42 | 26.87 | 20.33 | 6.54 | CL | 0.18 | 18.00 | 1.87 | 18.2 | 1.83 | 4.94 | 2.02 | 5.13 | 2.20 | 5.76 | 6.1 | 1.83 | 5.05 | 2.02 | 5.57 | 2.20 | 6.18 | 6.1 |
| 66 | 106+100 | 100 | 100 | 98.52 | 93.28 | 80.04 | 70.97 | 29.31 | 23.57 | 5.74 | CL | 0.15 | 15.00 | 1.93 | 18.7 | 1.88 | 6.39 | 2.07 | 6.58 | 2.25 | 7.39 | 6.4 | 1.88 | 6.53 | 2.07 | 7.15 | 2.25 | 7.93 | 7.7 |
| 67 | 107+000 | 100 | 100 | 98.62 | 93.38 | 74.77 | 66.22 | 30.43 | 20.31 | 10.12 | CL | 0.13 | 12.50 | 1.84 | 17.9 | 1.80 | 6.63 | 1.98 | 6.82 | 2.17 | 7.66 | 6.7 | 1.80 | 6.78 | 1.98 | 7.41 | 2.17 | 8.22 | 7.9 |

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|----|---------|-----|-----|-------|-------|-------|-------|-------|-------|-------|----|------|-------|------|------|------|------|------|------|------|------|-----|------|------|------|------|------|------|-----|
| 68 | 108+000 | 100 | 100 | 98.14 | 92.92 | 74.07 | 65.59 | 28.43 | 18.70 | 9.73 | CL | 0.11 | 11.00 | 1.86 | 18.1 | 1.82 | 6.71 | 2.01 | 6.89 | 2.19 | 7.75 | 6.8 | 1.82 | 6.85 | 2.01 | 7.49 | 2.19 | 8.31 | 8.0 |
| 69 | 109+000 | 100 | 100 | 97.51 | 92.33 | 73.07 | 57.54 | 25.46 | 17.01 | 8.45 | CL | 0.10 | 9.50 | 1.78 | 17.3 | 1.74 | 6.21 | 1.92 | 6.40 | 2.11 | 7.19 | 6.3 | 1.74 | 6.34 | 1.92 | 6.95 | 2.11 | 7.71 | 7.5 |
| 70 | 110+000 | 100 | 100 | 97.52 | 92.34 | 70.96 | 62.79 | 27.87 | 20.33 | 7.54 | CL | 0.18 | 18.00 | 1.66 | 16.8 | 1.46 | 5.30 | 1.68 | 6.40 | 1.83 | 6.90 | 7.0 | 1.46 | 5.41 | 1.68 | 6.96 | 1.83 | 7.40 | 7.0 |
| 71 | 111+000 | 100 | 100 | 98.25 | 93.03 | 83.96 | 74.5 | 29.53 | 22.75 | 6.78 | CL | 0.10 | 10.00 | 1.78 | 16.2 | 1.70 | 6.72 | 1.89 | 6.90 | 2.07 | 7.76 | 6.8 | 1.70 | 6.86 | 1.89 | 7.50 | 2.07 | 8.32 | 8.0 |
| 72 | 112+000 | 100 | 100 | 98.53 | 93.29 | 81.54 | 72.32 | 30.87 | 24.63 | 6.24 | CL | 0.19 | 18.50 | 1.85 | 16.9 | 1.77 | 5.97 | 1.96 | 6.15 | 2.15 | 6.91 | 6.0 | 1.77 | 6.10 | 1.96 | 6.69 | 2.15 | 7.42 | 7.2 |
| 73 | 113+000 | 100 | 100 | 97.51 | 92.33 | 75.04 | 66.47 | 31.43 | 25.67 | 5.76 | CL | 0.17 | 17.00 | 1.86 | 17.0 | 1.78 | 6.21 | 1.97 | 6.40 | 2.16 | 7.19 | 6.3 | 1.78 | 6.34 | 1.97 | 6.95 | 2.16 | 7.71 | 7.5 |
| 74 | 114+000 | 100 | 100 | 98.44 | 93.21 | 73.07 | 64.69 | 29.53 | 20.99 | 8.54 | CL | 0.16 | 16.00 | 1.87 | 17.1 | 1.79 | 6.71 | 1.98 | 6.89 | 2.17 | 7.75 | 6.8 | 1.79 | 6.85 | 1.98 | 7.49 | 2.17 | 8.31 | 8.0 |
| 75 | 115+000 | 100 | 100 | 98.33 | 93.1 | 87.63 | 77.8 | 28.54 | 18.30 | 10.24 | CL | 0.13 | 13.00 | 1.94 | 17.7 | 1.86 | 5.54 | 2.04 | 5.73 | 2.23 | 6.44 | 5.6 | 1.86 | 5.66 | 2.04 | 6.23 | 2.23 | 6.91 | 6.7 |
| 76 | 116+100 | 100 | 100 | 98.25 | 93.03 | 90.43 | 80.32 | 29.34 | 18.80 | 10.54 | CL | 0.15 | 15.00 | 1.78 | 16.2 | 1.70 | 5.13 | 1.89 | 5.32 | 2.07 | 5.97 | 6.5 | 1.70 | 5.24 | 1.89 | 5.78 | 2.07 | 6.41 | 6.3 |
| 77 | 117+150 | 100 | 100 | 98.90 | 96.57 | 90.01 | 73.27 | 28.41 | 20.18 | 8.23 | CL | 0.20 | 19.50 | 1.82 | 16.6 | 1.74 | 6.55 | 1.93 | 6.73 | 2.11 | 7.57 | 6.6 | 1.74 | 6.69 | 1.93 | 7.32 | 2.11 | 8.12 | 7.8 |
| 78 | 118+100 | 100 | 100 | 98.64 | 95.57 | 88.94 | 71.6 | 27.42 | 19.86 | 7.56 | CL | 0.12 | 12.00 | 1.94 | 17.7 | 1.86 | 5.78 | 2.04 | 5.96 | 2.23 | 6.70 | 5.8 | 1.86 | 5.90 | 2.04 | 6.48 | 2.23 | 7.19 | 7.0 |
| 79 | 119+000 | 100 | 100 | 99.05 | 87.94 | 87.56 | 72.33 | 27.42 | 19.86 | 7.56 | CL | 0.12 | 12.00 | 1.94 | 17.7 | 1.86 | 5.78 | 2.04 | 5.96 | 2.23 | 6.70 | 5.8 | 1.86 | 5.90 | 2.04 | 6.48 | 2.23 | 7.19 | 7.0 |
| 80 | 120+200 | 100 | 100 | 98.01 | 92.43 | 89.61 | 74.52 | 25.87 | 20.37 | 5.50 | CL | 0.10 | 10.00 | 1.64 | 16.5 | 1.55 | 4.70 | 1.72 | 7.60 | 1.83 | 8.60 | 6.1 | 1.55 | 4.80 | 1.72 | 8.26 | 1.83 | 9.23 | 7.9 |
| 81 | 121+150 | 100 | 100 | 99.60 | 96.7 | 87.83 | 72.18 | 26.33 | 19.63 | 6.70 | CL | 0.16 | 15.50 | 1.78 | 17.3 | 1.69 | 4.99 | 1.88 | 5.18 | 2.06 | 5.82 | 5.9 | 1.69 | 5.10 | 1.88 | 5.63 | 2.06 | 6.24 | 6.1 |
| 82 | 122+000 | 100 | 100 | 97.86 | 90.91 | 78.03 | 69.15 | 27.84 | 20.30 | 7.54 | CL | 0.11 | 11.00 | 1.74 | 16.9 | 1.65 | 6.43 | 1.84 | 6.62 | 2.02 | 7.44 | 6.5 | 1.65 | 6.57 | 1.84 | 7.19 | 2.02 | 7.98 | 7.7 |
| 83 | 123+000 | 100 | 100 | 98.53 | 91.54 | 87.63 | 77.79 | 26.85 | 19.20 | 7.65 | CL | 0.10 | 9.50 | 1.85 | 18.0 | 1.76 | 6.08 | 1.95 | 6.27 | 2.13 | 7.04 | 6.1 | 1.76 | 6.21 | 1.95 | 6.81 | 2.13 | 7.56 | 7.3 |
| 84 | 124+100 | 100 | 100 | 97.51 | 90.59 | 88.74 | 78.79 | 27.84 | 21.09 | 6.75 | CL | 0.09 | 8.50 | 1.82 | 17.7 | 1.73 | 5.73 | 1.92 | 5.92 | 2.10 | 6.65 | 5.8 | 1.73 | 5.86 | 1.92 | 6.43 | 2.10 | 7.14 | 6.9 |
| 85 | 125+100 | 100 | 100 | 98.61 | 95.55 | 80.91 | 71.09 | 27.41 | 20.14 | 7.27 | CL | 0.13 | 12.50 | 1.78 | 17.3 | 1.69 | 5.69 | 1.88 | 5.88 | 2.06 | 6.60 | 5.8 | 1.69 | 5.81 | 1.88 | 6.39 | 2.06 | 7.09 | 6.9 |
| 86 | 126+050 | 100 | 100 | 98.53 | 93.77 | 77.67 | 69.61 | 28.57 | 20.03 | 8.54 | CL | 0.11 | 11.00 | 1.93 | 18.7 | 1.83 | 6.64 | 2.02 | 6.83 | 2.21 | 7.67 | 6.7 | 1.83 | 6.79 | 2.02 | 7.42 | 2.21 | 8.23 | 7.9 |
| 87 | 127+000 | 100 | 100 | 98.22 | 95.33 | 80.43 | 72.12 | 29.87 | 22.42 | 7.45 | CL | 0.16 | 15.50 | 1.82 | 17.7 | 1.73 | 5.79 | 1.92 | 5.97 | 2.10 | 6.71 | 5.8 | 1.73 | 5.91 | 1.92 | 6.49 | 2.10 | 7.20 | 7.0 |
| 88 | 128+100 | 100 | 100 | 99.02 | 97.36 | 81.23 | 72.85 | 26.35 | 19.68 | 6.67 | CL | 0.17 | 16.50 | 1.76 | 17.1 | 1.67 | 5.49 | 1.86 | 5.68 | 2.04 | 6.38 | 5.6 | 1.67 | 5.61 | 1.86 | 6.17 | 2.04 | 6.84 | 6.7 |
| 89 | 129+000 | 100 | 100 | 99.14 | 96.44 | 82.65 | 74.14 | 31.54 | 22.11 | 9.43 | CL | 0.14 | 13.50 | 1.88 | 18.3 | 1.79 | 4.94 | 1.98 | 5.13 | 2.17 | 5.76 | 5.0 | 1.79 | 5.05 | 1.98 | 5.57 | 2.17 | 6.18 | 6.1 |
| 90 | 130+000 | 100 | 100 | 98.75 | 90.37 | 87.44 | 78.5 | 32.53 | 22.00 | 10.53 | CL | 0.10 | 10.00 | 1.72 | 16.7 | 1.52 | 5.40 | 1.76 | 5.70 | 1.94 | 5.90 | 5.5 | 1.52 | 5.52 | 1.76 | 6.20 | 1.94 | 6.33 | 6.5 |
| 91 | 131+150 | 100 | 100 | 98.23 | 96.7 | 87.44 | 78.5 | 27.03 | 19.92 | 7.11 | CL | 0.10 | 9.50 | 1.85 | 18.0 | 1.83 | 5.65 | 2.02 | 5.84 | 2.20 | 6.56 | 5.7 | 1.83 | 5.77 | 2.02 | 6.34 | 2.20 | 7.04 | 6.8 |

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|-----|---------|-----|-----|-------|-------|-------|-------|-------|-------|-------|------|------|-------|------|------|------|------|------|------|------|------|-----|------|------|------|------|------|------|-----|-----|
| 92 | 132+000 | 100 | 100 | 97.72 | 91.35 | 75.65 | 67.77 | 28.57 | 21.82 | 6.75 | CL | 0.10 | 9.50 | 1.84 | 17.9 | 1.82 | 6.01 | 2.01 | 6.20 | 2.19 | 6.96 | 6.1 | 1.82 | 6.14 | 2.01 | 6.73 | 2.19 | 7.47 | 7.2 | |
| 93 | 133+100 | 100 | 100 | 98.53 | 90.66 | 80.03 | 71.76 | 29.43 | 23.19 | 6.24 | CL | 0.11 | 11.00 | 1.79 | 17.4 | 1.77 | 6.13 | 1.96 | 6.31 | 2.14 | 7.09 | 6.2 | 1.77 | 6.26 | 1.96 | 6.86 | 2.14 | 7.61 | 7.4 | |
| 94 | 134+100 | 100 | 100 | 98.22 | 92.48 | 79.33 | 71.12 | 30.54 | 24.81 | 5.73 | CL | 0.12 | 12.00 | 1.78 | 17.3 | 1.76 | 5.97 | 1.94 | 6.15 | 2.13 | 6.91 | 6.0 | 1.76 | 6.10 | 1.94 | 6.69 | 2.13 | 7.42 | 7.2 | |
| 95 | 135+000 | 100 | 100 | 98.14 | 94.68 | 73.65 | 65.95 | 31.43 | 23.79 | 7.64 | CL | 0.17 | 17.00 | 1.93 | 18.7 | 1.91 | 5.57 | 2.09 | 5.75 | 2.28 | 6.46 | 5.6 | 1.91 | 5.68 | 2.09 | 6.25 | 2.28 | 6.93 | 6.7 | |
| 96 | 136+100 | 100 | 100 | 97.73 | 95.69 | 83.47 | 72.19 | 28.71 | 20.16 | 8.55 | CL | 0.22 | 21.50 | 1.85 | 18.0 | 1.83 | 5.80 | 2.02 | 5.98 | 2.20 | 6.72 | 5.9 | 1.83 | 5.92 | 2.02 | 6.50 | 2.20 | 7.21 | 7.0 | |
| 97 | 137+000 | 100 | 100 | 97.23 | 93.68 | 87.44 | 75.26 | 29.35 | 19.14 | 10.21 | CL | 0.20 | 20.00 | 1.78 | 17.3 | 1.76 | 6.60 | 1.94 | 6.79 | 2.13 | 7.63 | 6.7 | 1.76 | 6.74 | 1.94 | 7.38 | 2.13 | 8.18 | 7.9 | |
| 98 | 138+100 | 100 | 100 | 97.33 | 94.77 | 81.74 | 71.47 | 30.53 | 23.78 | 6.75 | CL | 0.20 | 20.00 | 1.77 | 17.2 | 1.75 | 6.64 | 1.93 | 6.83 | 2.12 | 7.67 | 6.7 | 1.75 | 6.79 | 1.93 | 7.42 | 2.12 | 8.23 | 7.9 | |
| 99 | 139+150 | 100 | 100 | 99.06 | 87.94 | 83.54 | 75.11 | 22.25 | 5.74 | 6.7 | 1.87 | 5.03 | 2.06 | 5.55 | 2.25 | 6.1 | | | | | | | | | | | | | 6 | 6.0 |
| 100 | 140+100 | 100 | 100 | 98.53 | 93.38 | 82.04 | 72.74 | 28.54 | 20.69 | 7.85 | CL | 0.15 | 15.00 | 1.70 | 13.0 | 1.49 | 6.00 | 1.69 | 6.60 | 1.87 | 6.90 | 6.4 | 1.49 | 6.13 | 1.69 | 7.17 | 1.87 | 7.40 | 7.4 | |
| 101 | 141+100 | 100 | 100 | 98.23 | 93.09 | 73.44 | 65 | 27.54 | 19.00 | 8.54 | CL | 0.09 | 9.45 | 1.81 | 17.6 | 1.79 | 5.10 | 1.97 | 5.29 | 2.16 | 5.94 | 5.2 | 1.79 | 5.21 | 1.97 | 5.74 | 2.16 | 6.37 | 6.2 | |
| 102 | 142+000 | 100 | 100 | 97.72 | 92.61 | 80.74 | 71.57 | 26.74 | 17.20 | 9.54 | CL | 0.15 | 15.00 | 1.83 | 17.8 | 1.81 | 4.92 | 2.00 | 5.11 | 2.18 | 5.74 | 5.0 | 1.81 | 5.03 | 2.00 | 5.55 | 2.18 | 6.16 | 6.0 | |
| 103 | 143+000 | 100 | 100 | 98.45 | 90.35 | 75.62 | 66.97 | 28.74 | 21.20 | 7.54 | CL | 0.11 | 11.00 | 1.86 | 18.1 | 1.84 | 5.22 | 2.03 | 5.40 | 2.21 | 6.07 | 5.3 | 1.84 | 5.33 | 2.03 | 5.87 | 2.21 | 6.51 | 6.4 | |
| 104 | 144+000 | 100 | 100 | 98.23 | 93.09 | 77.93 | 69.04 | 29.53 | 21.00 | 8.53 | CL | 0.13 | 13.00 | 1.79 | 17.4 | 1.77 | 5.57 | 1.95 | 5.75 | 2.14 | 6.46 | 5.6 | 1.77 | 5.68 | 1.95 | 6.25 | 2.14 | 6.93 | 6.7 | |
| 105 | 145+150 | 100 | 100 | 98.03 | 92.91 | 81.34 | 72.11 | 27.84 | 20.31 | 7.53 | CL | 0.10 | 10.00 | 1.78 | 17.3 | 1.76 | 5.65 | 1.94 | 5.84 | 2.13 | 6.56 | 5.7 | 1.76 | 5.77 | 1.94 | 6.34 | 2.13 | 7.04 | 6.8 | |
| 106 | 146+000 | 100 | 100 | 98.15 | 93.02 | 88.04 | 78.14 | 29.54 | 23.01 | 6.53 | CL | 0.12 | 12.00 | 1.74 | 16.9 | 1.72 | 6.00 | 1.90 | 6.18 | 2.09 | 6.95 | 6.1 | 1.72 | 6.13 | 1.90 | 6.72 | 2.09 | 7.46 | 7.2 | |
| 107 | 147+100 | 100 | 100 | 98.53 | 90.37 | 82.54 | 73.19 | 30.14 | 24.27 | 5.87 | CL | 0.19 | 19.00 | 1.85 | 18.0 | 1.83 | 6.60 | 2.02 | 6.79 | 2.20 | 7.63 | 6.7 | 1.83 | 6.74 | 2.02 | 7.38 | 2.20 | 8.18 | 7.9 | |
| 108 | 148+000 | 100 | 100 | 98.42 | 93.27 | 81.78 | 72.51 | 31.54 | 25.31 | 6.23 | CL | 0.09 | 9.00 | 1.86 | 18.1 | 1.84 | 6.63 | 2.03 | 6.82 | 2.21 | 7.66 | 6.7 | 1.84 | 6.78 | 2.03 | 7.41 | 2.21 | 8.22 | 7.9 | |
| 109 | 149+100 | 100 | 100 | 98.14 | 90.77 | 77.44 | 68.6 | 28.54 | 22.53 | 6.01 | CL | 0.08 | 8.00 | 1.82 | 17.7 | 1.80 | 5.95 | 1.99 | 6.13 | 2.17 | 6.89 | 6.0 | 1.80 | 6.07 | 1.99 | 6.66 | 2.17 | 7.39 | 7.2 | |
| 110 | 150+000 | 100 | 100 | 99.75 | 95.36 | 79.86 | 71.87 | 31.23 | 23.64 | 7.59 | CL | 0.13 | 13.00 | 1.68 | 12.7 | 1.54 | 8.10 | 1.68 | 5.90 | 1.96 | 6.00 | 5.8 | 1.54 | 8.27 | 1.68 | 6.41 | 1.96 | 6.44 | 7.5 | |
| 111 | 151+100 | 100 | 100 | 98.22 | 94.77 | 74.07 | 69.16 | 32.36 | 24.87 | 7.49 | CL | 0.18 | 18.00 | 1.78 | 16.4 | 1.69 | 6.60 | 1.87 | 6.79 | 2.06 | 7.63 | 6.7 | 1.69 | 6.74 | 1.87 | 7.38 | 2.06 | 8.18 | 7.9 | |
| 112 | 152+000 | 100 | 100 | 99.04 | 90.79 | 79.74 | 64.29 | 29.54 | 21.01 | 8.53 | CL | 0.20 | 20.00 | 1.86 | 17.2 | 1.77 | 6.75 | 1.95 | 6.94 | 2.14 | 7.79 | 6.8 | 1.77 | 6.90 | 1.95 | 7.54 | 2.14 | 8.36 | 8.1 | |
| 113 | 153+100 | 100 | 100 | 98.15 | 89.77 | 81.34 | 64.29 | 28.24 | 20.90 | 7.34 | CL | 0.13 | 13.00 | 1.84 | 17.0 | 1.75 | 6.21 | 1.93 | 6.40 | 2.12 | 7.19 | 6.3 | 1.75 | 6.34 | 1.93 | 6.95 | 2.12 | 7.71 | 7.5 | |
| 114 | 154+000 | 100 | 100 | 99.76 | 82.56 | 81.73 | 70.37 | 27.86 | 20.16 | 7.70 | CL | 0.14 | 13.50 | 1.78 | 16.4 | 1.69 | 6.28 | 1.87 | 6.47 | 2.06 | 7.27 | 6.3 | 1.69 | 6.42 | 1.87 | 7.03 | 2.06 | 7.80 | 7.5 | |
| 115 | 155+000 | 100 | 100 | 98.23 | 85.81 | 76.07 | 60.47 | 27.24 | 20.89 | 6.35 | CL | 0.18 | 18.00 | 1.83 | 16.9 | 1.74 | 5.58 | 1.92 | 5.76 | 2.11 | 6.47 | 5.6 | 1.74 | 5.70 | 1.92 | 6.26 | 2.11 | 6.95 | 6.8 | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----|---------|-----|-----|-------|-------|-------|-------|-------|-------|------|----|------|-------|------|------|------|------|------|------|------|------|-----|------|------|------|------|------|------|-----|
| 116 | 156+100 | 100 | 100 | 98.55 | 89.77 | 74.03 | 61.26 | 26.57 | 20.43 | 6.14 | CL | 0.13 | 13.00 | 1.84 | 17.0 | 1.75 | 5.57 | 1.93 | 5.75 | 2.12 | 6.46 | 5.6 | 1.75 | 5.68 | 1.93 | 6.25 | 2.12 | 6.93 | 6.7 |
| 117 | 157+000 | 100 | 100 | 98.45 | 87.47 | 79.74 | 69.16 | 28.54 | 20.01 | 8.53 | CL | 0.11 | 11.00 | 1.78 | 16.4 | 1.69 | 5.04 | 1.87 | 5.22 | 2.06 | 5.87 | 6.8 | 1.69 | 5.14 | 1.87 | 5.68 | 2.06 | 6.30 | 6.2 |
| 118 | 158+000 | 100 | 100 | 97.72 | 92.57 | 81.33 | 74.58 | 25.83 | 19.85 | 5.98 | CL | 0.14 | 13.50 | 1.77 | 16.3 | 1.68 | 5.12 | 1.86 | 5.31 | 2.05 | 5.96 | 6.7 | 1.68 | 5.23 | 1.86 | 5.77 | 2.05 | 6.40 | 6.3 |
| 119 | 159+100 | 100 | 100 | 97.33 | 90.77 | 83.74 | 69.6 | 26.87 | 19.03 | 7.84 | CL | 0.16 | 15.50 | 1.91 | 17.7 | 1.82 | 6.87 | 2.00 | 7.05 | 2.19 | 7.92 | 6.9 | 1.82 | 7.01 | 2.00 | 7.66 | 2.19 | 8.50 | 8.2 |
| 120 | 160+000 | 100 | 100 | 97.74 | 86.51 | 84.73 | 71.26 | 28.54 | 22.20 | 6.34 | CL | 0.10 | 10.00 | 1.65 | 12.3 | 1.55 | 6.10 | 1.71 | 6.90 | 1.86 | 7.10 | 6.8 | 1.55 | 6.23 | 1.71 | 7.50 | 1.86 | 7.62 | 7.6 |
| 121 | 161+00 | 100 | 100 | 97.14 | 86.06 | 76.72 | 64.27 | 29.14 | 23.38 | 5.76 | CL | 0.09 | 9.00 | 1.86 | 18.1 | 1.69 | 5.27 | 1.87 | 5.45 | 2.06 | 6.13 | 5.3 | 1.69 | 5.38 | 1.87 | 5.93 | 2.06 | 6.58 | 6.4 |
| 122 | 162+000 | 100 | 100 | 99.66 | 92.46 | 79.66 | 75.39 | 26.33 | 18.46 | 7.87 | CL | 0.09 | 8.50 | 1.84 | 17.9 | 1.67 | 5.04 | 1.85 | 5.22 | 2.04 | 5.87 | 5.1 | 1.67 | 5.14 | 1.85 | 5.68 | 2.04 | 6.30 | 6.2 |
| 123 | 163+000 | 100 | 100 | 98.64 | 89.48 | 79.52 | 75.97 | 27.44 | 18.57 | 8.87 | CL | 0.11 | 11.00 | 1.83 | 17.8 | 1.66 | 5.68 | 1.84 | 5.87 | 2.03 | 6.59 | 5.7 | 1.66 | 5.80 | 1.84 | 6.38 | 2.03 | 7.07 | 6.9 |
| 124 | 164+100 | 100 | 100 | 98.51 | 87.81 | 73.45 | 71.3 | 29.1 | 20.87 | 8.23 | CL | 0.13 | 13.00 | 1.84 | 17.9 | 1.67 | 6.60 | 1.85 | 6.79 | 2.04 | 7.63 | 6.7 | 1.67 | 6.74 | 1.85 | 7.38 | 2.04 | 8.18 | 7.9 |
| 125 | 165+000 | 100 | 100 | 99.55 | 95.6 | 80.93 | 74.59 | 28.61 | 20.36 | 8.25 | CL | 0.13 | 12.50 | 1.61 | 13.0 | 1.53 | 5.60 | 1.72 | 5.78 | 1.91 | 6.50 | 6.5 | 1.53 | 5.72 | 1.72 | 6.28 | 1.91 | 6.97 | 6.8 |
| 126 | 166+000 | 100 | 100 | 98.53 | 91.54 | 87.63 | 77.79 | 26.85 | 19.52 | 7.33 | CL | 0.11 | 11.00 | 1.65 | 14.9 | 1.56 | 6.20 | 1.75 | 6.39 | 1.93 | 7.18 | 6.2 | 1.56 | 6.33 | 1.75 | 6.94 | 1.93 | 7.70 | 7.4 |
| 127 | 167+000 | 100 | 100 | 97.51 | 90.59 | 88.74 | 78.79 | 27.84 | 21.09 | 6.75 | CL | 0.11 | 10.50 | 1.82 | 16.4 | 1.6 | 5.80 | 1.79 | 5.99 | 1.97 | 6.73 | 6.4 | 1.60 | 5.92 | 1.79 | 6.51 | 1.97 | 7.22 | 7.0 |
| 128 | 168+000 | 100 | 100 | 98.61 | 95.55 | 80.91 | 71.09 | 27.41 | 20.14 | 7.27 | CL | 0.12 | 12.00 | 1.60 | 14.4 | 1.62 | 6.45 | 1.81 | 6.64 | 1.99 | 7.46 | 6.5 | 1.62 | 6.59 | 1.81 | 7.21 | 1.99 | 8.00 | 7.7 |

9. BORROW AREA

All together Ten (10) Borrow Area sites are selected in consultation with concerned PWD engineers. These are near ch-41.000km to 48.500km, ch-63.50km, ch-71.500km, ch-75.00km, ch-82.200km, ch-92.480km, ch-100.000km, ch-108.000km, ch-134.980km & ch-147.000km. The soil types of all Borrow areas are of CI (Silty Clay) type.

The location of these borrow areas are shown below & the test results are summarized in table-9.1.

Some Photos of Borrow Areas at Different Locations are shown below:



(Near ch-45.000)



(Near ch-108.000)

Table: 9.1 TEST RESULTS OF BORROW AREA SOIL

| Sl. No. | Chainage (km) | Sieve Analysis (% Passing by Weight) | | | | | | Atterberg's Limit | | PI | Soil-Classification | Laboratory Compaction | | Soaked CBR at 3 Energy Levels | | | | | | Soaked CBR at 97% of MDD | Unsoaked CBR at 3 Energy Levels | | | | | | Unsoaked CBR at 97% of MDD | Swelling Index |
|---------|------------------|---|------------|------------|------------|----------|------------|----------------------|------------|-------|---------------------|--------------------------|------------|----------------------------------|------------|----------|------------|----------|------------|-----------------------------|------------------------------------|------|------|------|------|-------|-------------------------------|-------------------|
| | | MDD (gm/ cc) | OMC (%) | 10 Blows | | 35 Blows | | | | | | 65 Blows | | 10 Blows | | 35 Blows | | 65 Blows | | | | | | | | | | |
| | | | | DD | CBR (%) | DD | CBR (%) | DD | CBR (%) | | | DD | CBR (%) | DD | CBR (%) | DD | CBR (%) | DD | CBR (%) | | | | | | | | | |
| | | 20 mm | 10 mm | 4.75 mm | 2.36 mm | 600 μ | 75 μ | LL | PL | | | | | | | | | | | | | | | | | | | |
| 1 | 45.000 (RHS) | 100 | 100 | 99.95 | 95.64 | 87.3 | 72.29 | 32.52 | 22.8 | 9.72 | CL | 1.66 | 15.4 | 1.76 | 6.56 | 1.89 | 10.7 | 1.93 | 15.9 | 9.39 | 1.58 | 7.50 | 1.72 | 12.4 | 1.84 | 18.94 | 11.24 | 14.71 |
| 2 | 63.500 (LHS) | 100 | 100 | 98.83 | 94.21 | 88.6 | 71.34 | 31.74 | 22.26 | 9.48 | CL | 1.70 | 15.4 | 1.78 | 6.91 | 1.91 | 8.8 | 1.97 | 13.9 | 8.59 | 1.60 | 7.90 | 1.74 | 10.1 | 1.88 | 16.51 | 10.28 | 13.99 |
| 3 | 71.500 (LHS) | 100 | 100 | 99.6 | 98.76 | 82.39 | 71.96 | 30.88 | 20.87 | 10.00 | CL | 1.67 | 14.7 | 1.8 | 7.17 | 1.94 | 10.0 | 1.95 | 15.9 | 8.66 | 1.62 | 8.20 | 1.76 | 11.6 | 1.86 | 18.92 | 10.36 | 14.80 |
| 4 | 75.000 (LHS) | 100 | 100 | 99.05 | 92.34 | 87.97 | 73.88 | 31.72 | 22.79 | 8.93 | CL | 1.63 | 14.5 | 1.74 | 8.22 | 1.88 | 11.4 | 1.91 | 15 | 10.5 | 1.56 | 9.40 | 1.71 | 13.2 | 1.82 | 17.83 | 12.58 | 15.16 |
| 5 | 82.200 (LHS) | 100 | 100 | 98.79 | 93.25 | 88.59 | 71.18 | 29.51 | 22.98 | 6.53 | CL | 1.66 | 15.6 | 1.71 | 6.65 | 1.85 | 10.8 | 1.98 | 13.9 | 8.25 | 1.54 | 7.60 | 1.68 | 12.4 | 1.89 | 16.47 | 9.87 | 16.70 |
| 6 | 92.480 (LHS) | 100 | 100 | 98.83 | 94.21 | 88.6 | 71.34 | 31.7 | 21.18 | 10.52 | CL | 1.60 | 15.6 | 1.79 | 6.04 | 1.88 | 12.0 | 1.91 | 14.7 | 9.59 | 1.61 | 6.90 | 1.71 | 13.9 | 1.82 | 17.42 | 11.48 | 14.80 |
| 7 | 100.050 (LHS) | 100 | 100 | 98.8 | 93.61 | 79.51 | 74.23 | 31.38 | 22.31 | 9.07 | CL | 1.68 | 14.7 | 1.8 | 5.97 | 1.91 | 9.7 | 1.94 | 15.5 | 10.3 | 1.62 | 6.82 | 1.74 | 11.3 | 1.85 | 18.47 | 12.34 | 17.87 |
| 8 | 108.00 (LHS) | 100 | 100 | 99.83 | 93.47 | 87.59 | 72.9 | 32.96 | 23.71 | 9.25 | CL | 1.61 | 14.7 | 1.82 | 6.26 | 1.96 | 9.0 | 1.96 | 14.2 | 9.42 | 1.64 | 7.16 | 1.78 | 10.4 | 1.87 | 16.93 | 11.28 | 19.86 |
| 9 | 134.980 (LHS) | 100 | 100 | 98.4 | 90.16 | 89.57 | 68.94 | 31.62 | 23.26 | 8.36 | CL | 1.65 | 15.6 | 1.77 | 7.21 | 1.96 | 9.9 | 1.92 | 14.7 | 9.81 | 1.59 | 8.24 | 1.78 | 11.5 | 1.83 | 17.42 | 11.74 | 19.49 |
| 10 | 147.000 (LHS) | 100 | 100 | 99.96 | 93.06 | 79.71 | 72.04 | 32.31 | 23.59 | 8.72 | CL | 1.68 | 15.0 | 1.81 | 7.66 | 1.94 | 10.7 | 1.95 | 13.9 | 10.6 | 1.63 | 8.76 | 1.76 | 12.4 | 1.86 | 16.48 | 12.69 | 15.25 |

10. MATERIAL QUARRY

LOCATION: BIPIN QUARRY: It is on 32.00km of NH36. Which is 3km lead to the approach road of NH36. From there it is 7.70km to the project road. It is on LHS of NH36.

| Location and name of quarry if any (correlated with index map) | Type of Rock (General group, classification or trade name) | Specimen No. | Los-Angeles Abrasion Value (IS 2386 Part-IV) | Aggregate Impact Value | | Water Absorptions (IS 2386 Part III) | Flakiness Index *** (IS 2386 Part I) | | Elongation Index | | Combine Flakiness and Elongation Index | | Soundness test | Stripping Value *** (IS 6241) | Remarks regarding performance of the aggregate wherever a systematic evaluation has been made | Addl. Remarks, like, old/new quarry, approximate quantity available, existing access to quarry, etc. |
|--|--|--------------|--|----------------------------|--------------------|--------------------------------------|--------------------------------------|--------------------|--------------------|--------------------|--|--------------------|--|-------------------------------|---|--|
| | | | | Dry test (IS 2386 Part-IV) | Wet test (IS 5640) | | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | Loss of aggregate after 10cycle immersion in sodium sulphate solution (IS2386-partV) (%) | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | | | | | | 10 | 11 | 12 |
| BIPIN QUARRY | Sandstone | 1 | 19.5 | 14 | 15 | 0.56 | 15.3 | 12.35 | 12.84 | 16.58 | 28.14 | 28.93 | 7 | 4 | Satisfactory | Satisfactory |
| | Sandstone | 2 | 19.2 | 12 | 16 | 0.53 | 15.64 | 12.15 | 12.2 | 16.68 | 27.84 | 28.83 | 7.5 | 4 | Satisfactory | Satisfactory |
| | Sandstone | 3 | 20.5 | 13 | 17 | 0.59 | 15.25 | 12.45 | 12.64 | 16.25 | 27.89 | 28.7 | 7 | 4 | Satisfactory | Satisfactory |
| | | Average | | 19.73 | 13.00 | 16.00 | 0.56 | 15.40 | 12.32 | 12.56 | 16.50 | 27.96 | 28.82 | 7.17 | 4.00 | |

LOCATION: LONGNIT QUARRY: It is on 147.00km of NH36. This is at a leading distance of 3km from NH36. It is in the right side of NH.36.

| Location and name of quarry if any (correlated with index map) | Type of Rock (General group, classification or trade name) | Specimen No. | Los-Angeles Abrasion Value (IS 2386 Part-IV) | Aggregate Impact Value | | Water Absorptions (IS 2386 Part III) | Flakiness Index *** (IS 2386 Part I) | | Elongation Index | | Combine Flakiness and Elongation Index | | Soundness test Loss of aggregate after 10cycle immersion in sodium sulphate solution (IS2386-partV) (%) | Stripping Value *** (IS 6241) | Remarks regarding performance of the aggregate wherever a systematic evaluation has been made | Addl. Remarks, like, old/new quarry, approximate quantity available, existing access to quarry, etc. |
|--|--|--------------|--|----------------------------|--------------------|--------------------------------------|--------------------------------------|--------------------|--------------------|--------------------|--|--------------------|--|-------------------------------|---|--|
| | | | | Dry test (IS 2386 Part-IV) | Wet test (IS 5640) | | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | | | | | 10 | 11 | 12 | |
| LONGNIT QUARRY | Sandstone | 1 | 20.25 | 13 | 16 | 0.54 | 15.25 | 12.56 | 12.25 | 15.94 | 27.5 | 28.5 | 7.5 | 3 | Satisfactory | Satisfactory |
| | Sandstone | 2 | 19.6 | 14 | 17 | 0.62 | 14.89 | 11.95 | 11.85 | 16.25 | 26.74 | 28.2 | 7.6 | 5 | Satisfactory | Satisfactory |
| | Sandstone | 3 | 21.65 | 13 | 15 | 0.52 | 15.46 | 12.24 | 12.94 | 16.84 | 28.4 | 29.08 | 7.5 | 4 | Satisfactory | Satisfactory |
| | Average | | | 20.50 | 13.33 | 16.00 | 0.56 | 15.20 | 12.25 | 12.35 | 16.34 | 27.55 | 28.59 | 7.53 | 4.00 | |

LOCATION: FAIJONG QUARRY: It is on 147.00km of NH36. This is at a leading distance of 15km from NH36.

| Location and name of quarry if any (correlated with index map) | Type of Rock (General group, classification or trade name) | Specimen No. | Los-Angeles Abrasion Value (IS 2386 Part-IV) | Aggregate Impact Value | | Water Absorptions (IS 2386 Part III) | Flakiness Index *** (IS 2386 Part I) | | Elongation Index | | Combine Flakiness and Elongation Index | | Soundness test | Stripping Value *** (IS 6241) | Remarks regarding performance of the aggregate wherever a systematic evaluation has been made | Addl. Remarks, like, old/new quarry, approximate quantity available, existing access to quarry, etc. |
|--|--|--------------|--|----------------------------|--------------------|--------------------------------------|--------------------------------------|--------------------|--------------------|--------------------|--|--------------------|--|-------------------------------|---|--|
| | | | | Dry test (IS 2386 Part-IV) | Wet test (IS 5640) | | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | Loss of aggregate after 10cycle immersion in sodium sulphate solution (IS2386-partV) (%) | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | | | | | | 10 | 11 | 12 |
| FAIJONG QUARRY | Sandstone | 1 | 19.56 | 14 | 15 | 0.56 | 15.25 | 12.56 | 11.85 | 16.24 | 27.1 | 28.8 | 7 | 4 | Satisfactory | Satisfactory |
| | Sandstone | 2 | 21.54 | 13 | 15 | 0.58 | 14.89 | 12.89 | 13.29 | 15.75 | 28.18 | 28.64 | 7.2 | 4 | Satisfactory | Satisfactory |
| | Sandstone | 3 | 20.48 | 15 | 15 | 0.53 | 15.46 | 12.24 | 12.45 | 15.84 | 27.91 | 28.08 | 7.1 | 4 | Satisfactory | Satisfactory |
| | Average | | | 20.53 | 14.00 | 15.00 | 0.56 | 15.20 | 12.56 | 12.53 | 15.94 | 27.73 | 28.51 | 7.10 | 4.00 | |

LOCATION: LISUGHAT QUARRY: It is at a distance of 15km from Dimapur

| Location and name of quarry if any (correlated with index map) | Type of Rock (General group, classification or trade name) | Specimen No. | Los-Angeles Abrasion Value (IS 2386 Part-IV) | Aggregate Impact Value | | Water Absorptions (IS 2386 Part III) | Flakiness Index *** (IS 2386 Part I) | | Elongation Index | | Combine Flakiness and Elongation Index | | Soundness test Loss of aggregate after 10cycle immersion in sodium sulphate solution (IS2386-partV) (%) | Stripping Value *** (IS 6241) | Remarks regarding performance of the aggregate wherever a systematic evaluation has been made | Addl. Remarks, like, old/new quarry, approximate quantity available, existing access to quarry, etc. |
|--|--|--------------|--|----------------------------|--------------------|--------------------------------------|--------------------------------------|--------------------|--------------------|--------------------|--|--------------------|--|-------------------------------|---|--|
| | | | | Dry test (IS 2386 Part-IV) | Wet test (IS 5640) | | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | Nominal Size 40 mm | Nominal Size 20 mm | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | | | | | | 10 | 11 | 12 |
| LISUGHAT QUARRY | Sandstone | 1 | 19.56 | 13 | 14 | 0.54 | 15.26 | 12.25 | 11.87 | 15.24 | 27.13 | 27.49 | 7.5 | 3 | Satisfactory | Satisfactory |
| | Sandstone | 2 | 19.26 | 14 | 13 | 0.52 | 14.75 | 12.36 | 12.35 | 15.75 | 27.1 | 28.11 | 7 | 5 | Satisfactory | Satisfactory |
| | Sandstone | 3 | 19 | 15 | 13 | 0.58 | 15.35 | 12.87 | 12.68 | 15.62 | 28.03 | 28.49 | 7.3 | 4 | Satisfactory | Satisfactory |
| | Average | | | 19.27 | 14.00 | 13.33 | 0.55 | 15.12 | 12.49 | 12.30 | 15.54 | 27.42 | 28.03 | 7.27 | 4.00 | |

10.1: LABORATORY TEST REPORT ON FINE AGGREGATE SAND

LOCATION: Doboka Sand Mahal- It is on 40km of NH36. It is a roadside quarry and RHS of NH36.

| Name of quarry | Specimen No. | Sieve Analysis % Passing | | | | | | | Silt and Clay | Fineness Modulus | Zone | Water absorptions (IS:2386 Part III) | Specific Gravity | Deleterious Material Contents | Remarks / performance of the aggregate wherever evaluation has been made |
|--------------------------|--------------|--------------------------|---------|---------|---------|---------|---------|--------|---------------|------------------|------|--------------------------------------|------------------|-------------------------------|--|
| | | 4.75 mm | 2.36 mm | 1.18 mm | 600 mic | 300 mic | 150 mic | 75 mic | | | | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| Doboka Sand Mahal | Sample - 1 | 100.00 | 100.00 | 98.25 | 92.12 | 46.15 | 4.32 | 1.04 | 1.04 | 1.04 | IV | 0.29 | 2.64 | Nil | Sub-base and embankment filling works. |
| | Sample - 2 | 100.00 | 100.00 | 98.20 | 91.58 | 45.48 | 3.75 | 0.92 | 0.92 | 1.35 | IV | 0.28 | 2.63 | Nil | |
| | Sample - 3 | 100.00 | 100.00 | 99.05 | 91.90 | 44.25 | 3.60 | 0.93 | 0.93 | 1.41 | IV | 0.30 | 2.65 | Nil | |

LOCATION: Sarakati Sand Mahal- It is on 70km of NH36. It is also a roadside Quarry and RHS of NH36.

| Name of quarry | Specimen No. | Sieve Analysis % Passing | | | | | | | Silt and Clay | Fineness Modulus | Zone | Water absorptions (IS:2386 Part III) | Specific Gravity | Deleterious Material Contents | Remarks / performance of the aggregate wherever evaluation has been made |
|----------------------------|--------------|--------------------------|---------|---------|---------|---------|---------|--------|---------------|------------------|------|--------------------------------------|------------------|-------------------------------|--|
| | | 4.75 mm | 2.36 mm | 1.18 mm | 600 mic | 300 mic | 150 mic | 75 mic | | | | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| Sarakati Sand Mahal | Sample - 1 | 100.00 | 100.00 | 99.25 | 94.56 | 44.82 | 3.26 | 0.95 | 0.95 | 1.45 | IV | 0.29 | 2.66 | Nil | Sub-base and embankment filling works. |
| | Sample - 2 | 100.00 | 100.00 | 98.35 | 91.35 | 45.37 | 3.50 | 0.89 | 0.89 | 1.52 | IV | 0.34 | 2.63 | Nil | |
| | Sample - 3 | 100.00 | 100.00 | 97.80 | 92.57 | 46.50 | 3.45 | 1.01 | 1.01 | 1.30 | IV | 0.26 | 2.64 | Nil | |

LOCATION: Longnit River Quarry- It is on 121.00km of NH36. It required a 3km lead from RHS of NH36.

| Name of quarry | Specimen No. | Sieve Analysis % Passing | | | | | | | Silt and Clay | Fineness Modulus | Zone | Water absorptions (IS:2386 Part III) | Specific Gravity | Deleterious Material Contents | Remarks / performance of the aggregate wherever evaluation has been made |
|----------------------|--------------|--------------------------|---------|---------|---------|---------|---------|--------|---------------|------------------|------|--------------------------------------|------------------|-------------------------------|--|
| | | 4.75 mm | 2.36 mm | 1.18 mm | 600 mic | 300 mic | 150 mic | 75 mic | | | | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| Longnit River Quarry | Sample - 1 | 100.00 | 100.00 | 98.25 | 93.54 | 44.23 | 3.28 | 0.84 | 84 | 1.58 | IV | 0.35 | 2.60 | Nil | Sub-base and embankment filling works. |
| | Sample - 2 | 100.00 | 100.00 | 97.36 | 93.85 | 46.57 | 4.05 | 0.92 | 0.92 | 1.45 | IV | 0.31 | 2.64 | Nil | |
| | Sample - 3 | 100.00 | 100.00 | 98.65 | 92.78 | 44.65 | 3.74 | 1.04 | 1.04 | 1.42 | IV | 0.28 | 2.65 | Nil | |

11. WATER SOURCE

Samples of potable water from Silveta river source were collected. It is on 108.00km to 114.00km and RHS of Nh36. The tests were carried out as described in IS: 456:2000 to ascertain the quality of water for construction work as per following:

- To neutralize 200 ml sample of water, using phenolphthalein as an indicator, it should not require more than 2 ml of 0.1 normal NaOH.
- To neutralize 200 ml sample of water, using methyl orange as an indicator, it should not require more than 10 ml of 0.1 normal HCl.
- The permissible limits for solids shall be as follows when tested in accordance with IS: 3025:

Solids Permissible Limits (max)

Organic 200 mg/lit

Inorganic 3000 mg/lit

Sulphates (SO₄) 500 mg/lit

Chlorides (Cl) 500 mg/lit *

Suspended matter 2000 mg/lit

*Note: In case of structures of lengths 30 m and below, the permissible limit of chlorides may be increased up to 1000 mg/lit.

- The pH value shall not be less than 6; it is preferable to have pH value 7.

The sample test results are given in Table 11.1, which gives an indication of the nature and quality of the sub-surface water in the underlying aquifer only.

11.1 Analysis of Test Results:

The Test results are given in Table: 11.1 below. The laboratory test results reveal that the amount of chloride and sulphates present are well below the permissible limit of 500 mg/litre. Moreover the pH of the water is also > 6.0. Suspended solid matter is also below the limiting value of 2000 mg /litre.

Since the sources are potable, the presence of organic matter as tested gave negative results; minimal amount of organic impurities observed. Thus, it can be summarized that the nature and quality of water available from the sources as identified, collected and tested by the consultant, is good and fit for construction for the pavement and concrete purpose.

Table: 11.1 LABORATORY TEST REPORT ON WATER SOURCES

| Location | Nature of Source | Name of Test | | | | | | | |
|------------------|------------------|--------------|--|--|--|------------------|-----------------------------|----------------|------------------|
| | | pH Value | Quantity of 0.02 N NaOH solution required to neutralize 100mm of water sample using phenolphthalein as indicator | Quantity of 0.02 NH ₂ SO ₄ solution required to neutralize 100mm of water sample using mixed indicator | Organic Matter in terms of Oxygen absorbed by acid permanganate solution | Inorganic solids | Sulphate as SO ₄ | Chloride as Cl | Suspended Solids |
| (km) | | | (ml) | (ml) | (mg/l) | (mg/l) | (mg/l) | (mg/l) | (mg/l) |
| 108.00 to 114.00 | River source | 6.7 | 4.2 | 4.1 | 0.14 | 47 | 225 | 5.7 | 1028 |

12. Bitumen

The bitumen shall be harder grade paving bitumen of penetration grade 80/100 or 60/70 as directed by the engineer-in-charge complying with IS: 73 for paving bitumen requirements. The nearest source of bitumen supply is IOCL refinery and the binder for prime and tack coat shall be bituminous emulsion complying with specification IS 8887 as available in Guwahati.

Bitumen test

1. Specific gravity = 0.96